

Evaluation of J_{nr} Criterion for Unmodified Asphalt Binders

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Asphalt Binder Expert Task Group Meeting

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 - Michael Arasteh, AOTR
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 - Technical Advisory Committee



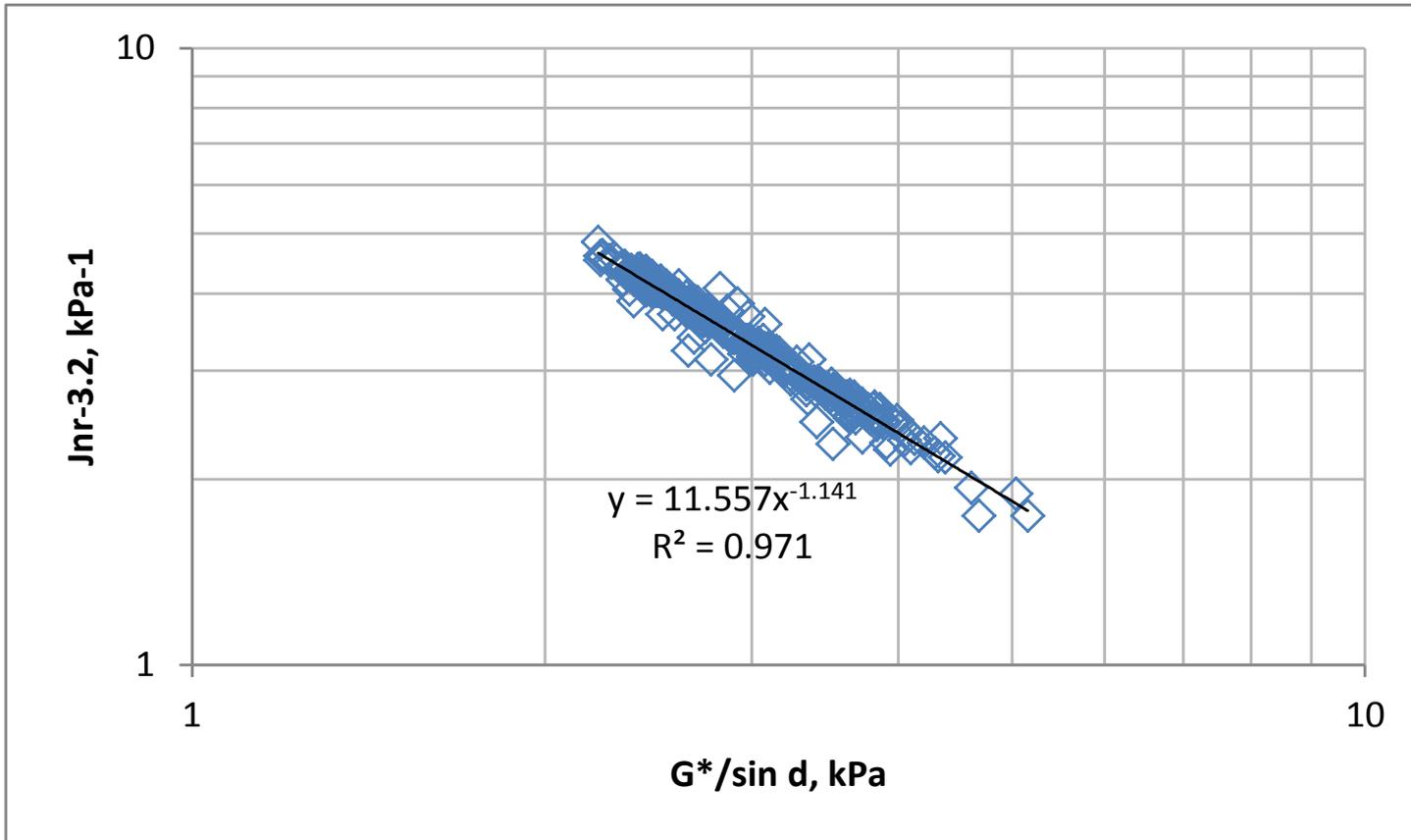
Evaluation of Straight run binders

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Sample ID	Name	Grade	true grade	Temp	Jnr 3.2kPa
ALF 6727	Control	70-22	72.7-74.2	72.7	4.39
BBRS3	straight	64-22	66.1-27.3	66.1	4.18
MN county rd 112	neat Valero	58-28	60.8-33.4	60.8	3.68
MN county rd 112	neat Citgo	58-28	59.5-29.8	59.5	5.30
MN county rd 112	AshlandM	58-28	60.7-31.4	60.7	4.30
Minn Road	straight	58-28	61.8-30.8	61.8	3.03
Miss I-55	CSL	67-22	68.3-25.1	68.3	2.67
Shandong	straight	64-22	64.4-23.5	64.4	4.44
BBRS3	straight	70-22	71.4-24.8	71.4	4.81
BBRS3	straight	58-28	61.3-30	61.3	4.00
MD project	straight	64-28	64.8-29.6	64.8	4.59
average					4.13



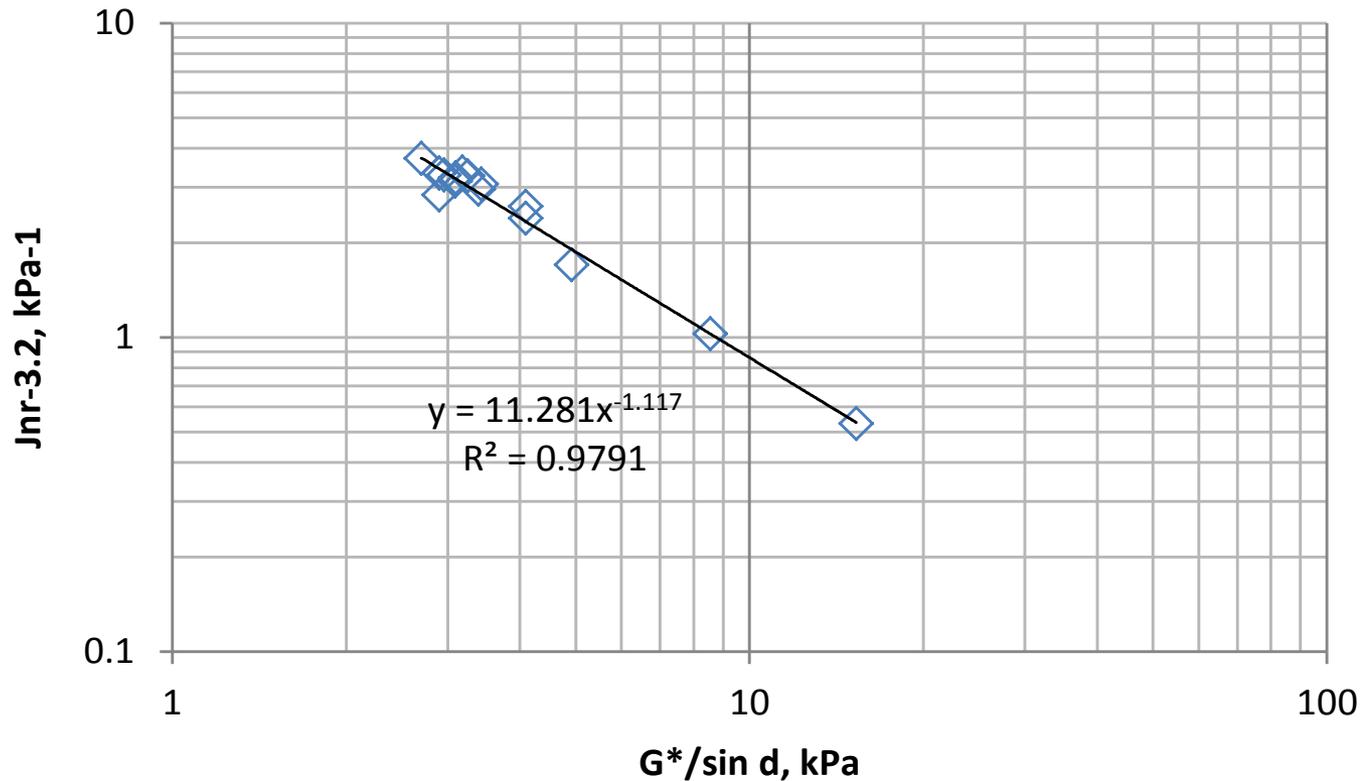
Unmodified Asphalt Binders: Source A



A	11.557
B	-1.141
G*/sin d	2.2
Jnr-3.2	4.700
Jnr-3.2	4
G*/sin d	2.53



Unmodified Asphalt Binders: AI MSCR Database



A	11.281
B	-1.117
G*/sin δ	2.2
Jnr-3.2	4.676
Jnr-3.2	4
G*/sin δ	2.53



Summary

- Criterion for unmodified asphalt binders may need to change?
 - $J_{nr} = 4.00 \text{ kPa}^{-1}$ equates to $G^*/\sin \delta$ value of 2.53 kPa
 - Could be problem for some unmodified asphalt binders
- If “S” grade criterion changes, do we change criterion for other AASHTO MP19 grades?



MRL Asphalt Binders

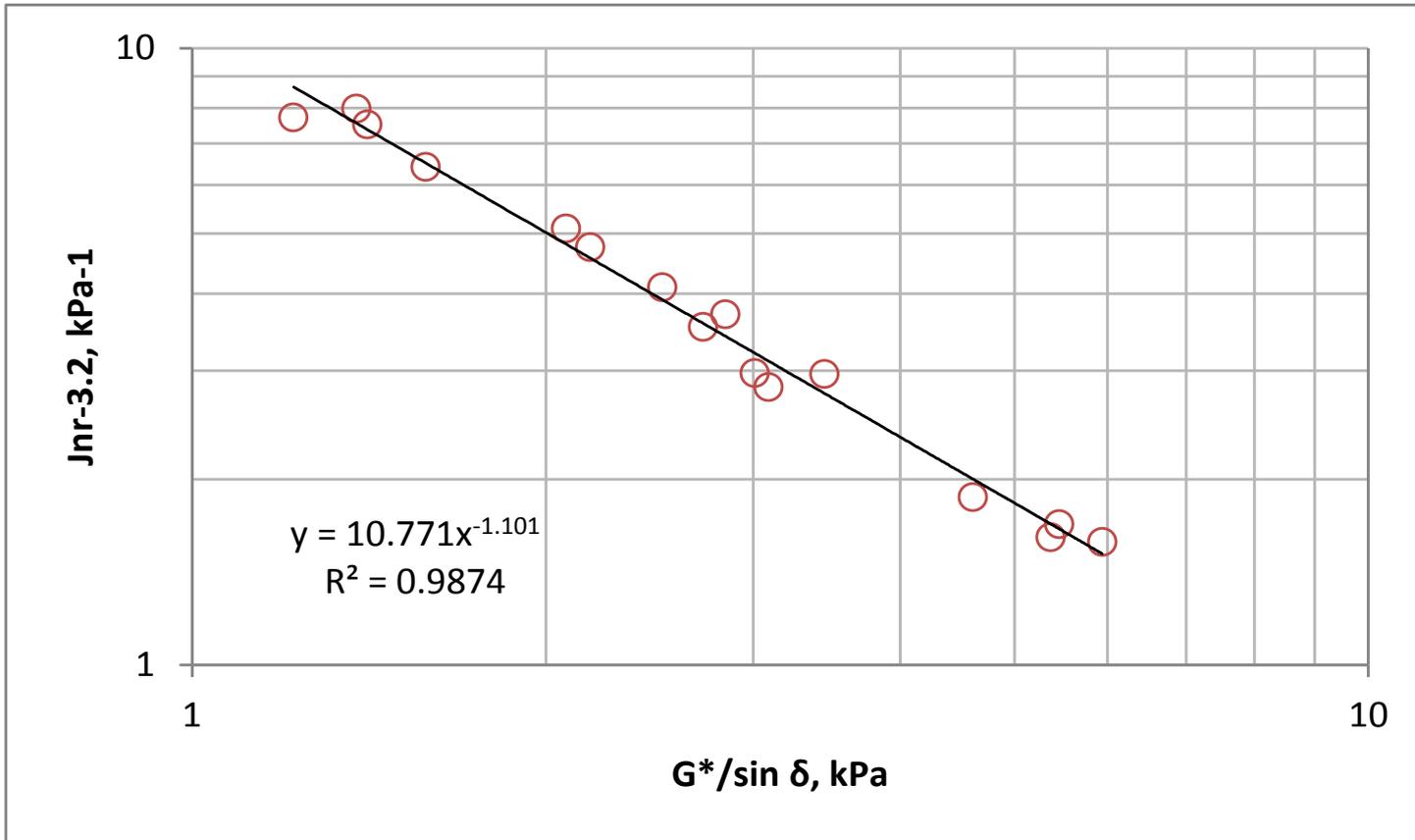
Comparison of Jnr and $G^*/\sin \delta$

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	AAA	AAB	AAC	AAD	AAF	AAG	AAK	AAM
MSCR Jnr-3.2, kPa^{-1}								
58°C	2.97	1.87	2.82	1.61		1.69		
64°C	7.52	5.10	7.98	4.09	3.70	4.75	1.58	2.96
70°C					7.71		3.53	6.41
RTFO DSR $G^*/\sin \delta$, kPa								
58°C	3.01	4.61	3.09	5.37		5.46		
64°C	1.41	2.08	1.38	2.51	2.84	2.18		3.45
70°C				1.20	1.22		2.72	1.58
T_c Jnr-3.2 = 4.0 kPa^{-1}	59.9	62.5	60.0	63.9	64.6	63.0	70.9	66.3
T_c $G^*/\sin \delta = 2.20 \text{ kPa}$	60.5	63.6	60.5	65.1	65.8	63.9	71.8	67.5



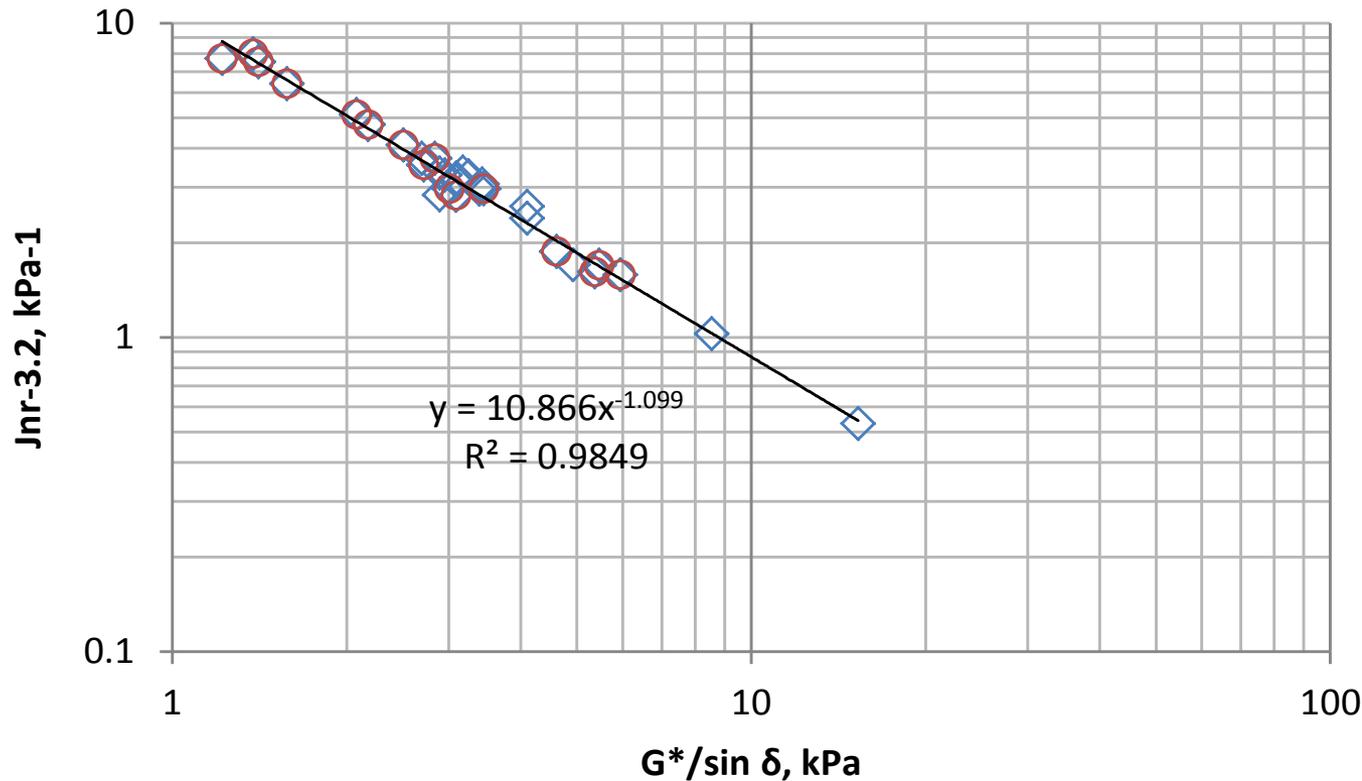
MRL Asphalt Binders



A	10.771
B	-1.101
$G^*/\sin \delta$	2.2
$J_{nr-3.2}$	4.521
$J_{nr-3.2}$	4
$G^*/\sin \delta$	2.46



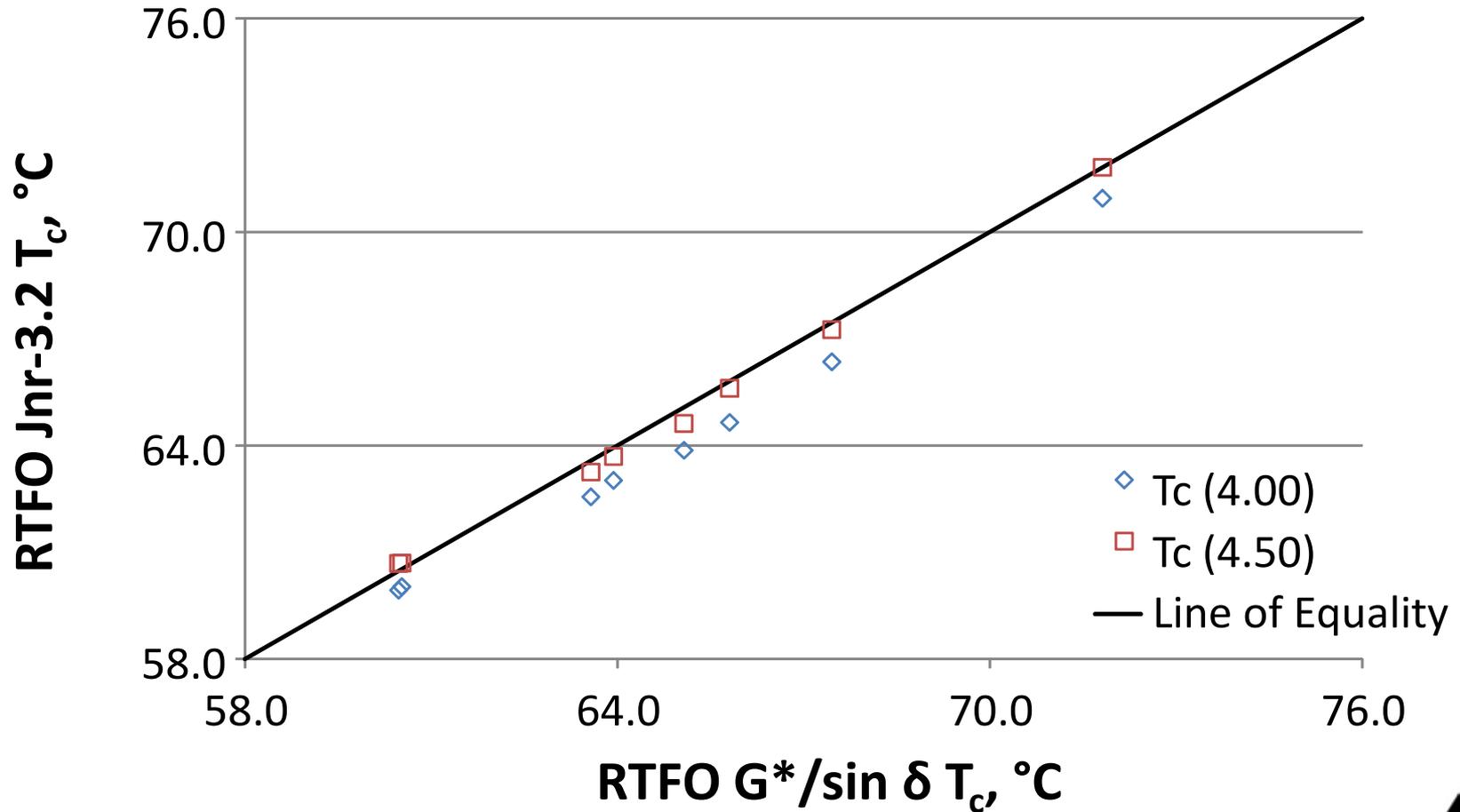
Unmodified Asphalt Binders: AI MSCR Database



A	10.866
B	-1.099
$G^*/\sin \delta$	2.2
$J_{nr-3.2}$	4.568
$J_{nr-3.2}$	4
$G^*/\sin \delta$	2.48



MRL Asphalt Binders



TAC Evaluation of SHRP MRL Asphalt Binders

- Purpose
 - (1) to provide additional data to the Asphalt Binder Expert Task Group (ETG) to evaluate if the 4.0 kPa^{-1} criterion for unmodified asphalt binders (“S” grades in AASHTO MP19) needs to be changed; and
 - (2) to evaluate if there is a bias in MSCR results dependent on DSR manufacturer



TAC Evaluation of SHRP MRL Asphalt Binders

- Task Force formed at TAC Meeting in April 2012 (Baltimore)
 - Seven Labs
 - PRI Asphalt Technologies
 - Asphalt Technologies Group (Meigs)
 - Jebro (2)
 - Flint Hills Resources
 - MTE (3)
 - FHWA (2)
 - Asphalt Institute



TAC Evaluation of SHRP MRL Asphalt Binders

- 11 Dynamic Shear Rheometers
 - Anton Paar
 - Smartpave (5)
 - TA Instruments
 - AR-2000 (3)
 - AR-G2 (1)
 - DHR-3 (1)
 - Malvern
 - Kinexus (1)



TAC Evaluation of SHRP MRL Asphalt Binders

- SHRP MRL Asphalt Binders
 - AAA Lloydminster 150/200 (PG 58-28)
 - AAB WY Sour AC-10 (PG 58-22)
 - AAC Redwater AC-8 (PG 58-16)
 - AAD CA Coastal AR-4000 (PG 58-28)
 - AAF West TX Sour AC-20 (PG 64-10)
 - AAG CA Valley AR-4000 (PG 58-10)
 - AAK Boscan AC-30 (PG 64-22)
 - AAM West TX Intermediate AC-20 (PG 64-16)



TAC Evaluation of SHRP MRL Asphalt Binders

- Test Temperatures
 - AAA, AAB, AAC, AAD, AAG
 - 58, 64C
 - AAF, AAK, AAM
 - 64, 70C
- AASHTO T315
 - $G^*/\sin \delta$
 - T_c (where $G^*/\sin \delta = 2.20$ kPa)
 - $G^*/\sin \delta @ T_{c,Jnr-3.2}$
- AASHTO TP70
 - Jnr-3.2
 - T_c (where $Jnr-3.2 = 4.00$ kPa⁻¹)
 - Jnr-3.2 @ $T_{c,G^*/\sin \delta}$



TAC Evaluation of SHRP MRL Asphalt Binders

- Labs receive 3 tins (1-oz) of RTFO-aged binder
 - 6 of 8 asphalt binders received
 - Resulted in 6-9 evaluations of each MRL asphalt binder
- Use one tin for TP70 at each temperature
 - Do not reheat sample
- Use one tin for T315 at both temperatures
 - Alternatively, pour sample and run T315 followed by TP70 at one temperature

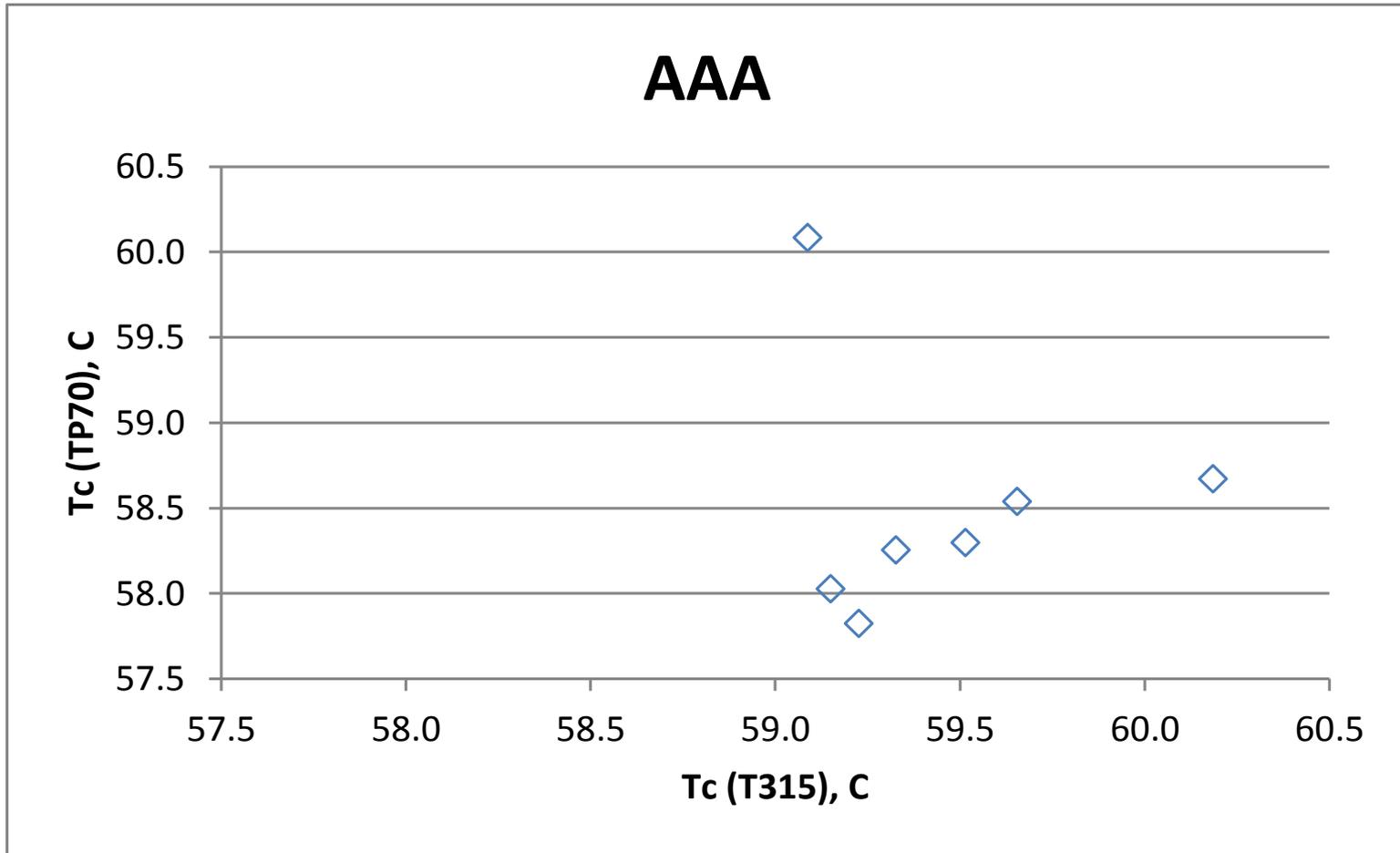


Data

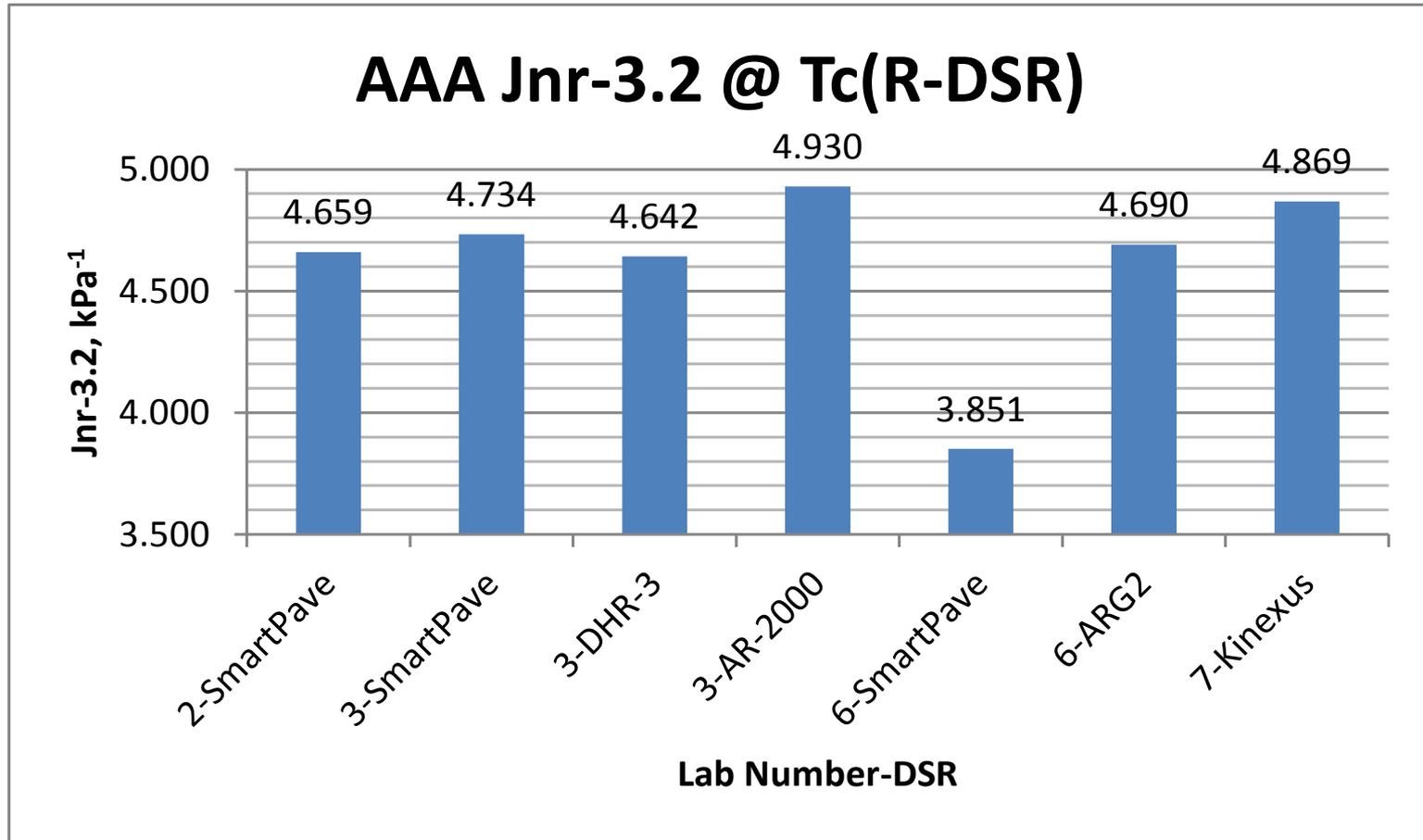
			1-AR2000	2-SmartPa	3-SmartPa	3-DHR-3	3-AR-2000	4-TA	4-SmartPa
AAC	G*/sin δ	58	3.26	2.35	3.19	3.20	3.34	2.88	3.06
		64	1.31	0.96	1.31	1.31	1.41	1.24	1.27
		T _c	60.6	58.4	60.5	60.5	60.9	59.9	60.3
	J _{nr-3.2}	58	3.399	4.310	3.488	3.467	3.298	3.632	3.479
		64	8.929	10.756	9.033	9.039	8.591	9.094	9.033
		T _c	59.0	57.5	58.9	58.9	59.2	58.6	58.9
		T _{R-DSR}	5.155	4.610	5.189	5.183	5.240	4.864	4.977
		T _{Jnr-3.2}	2.79	2.53	2.81	2.80	2.80	2.63	2.69



Comparison of T_c Determined by TP70 and T315: AAA

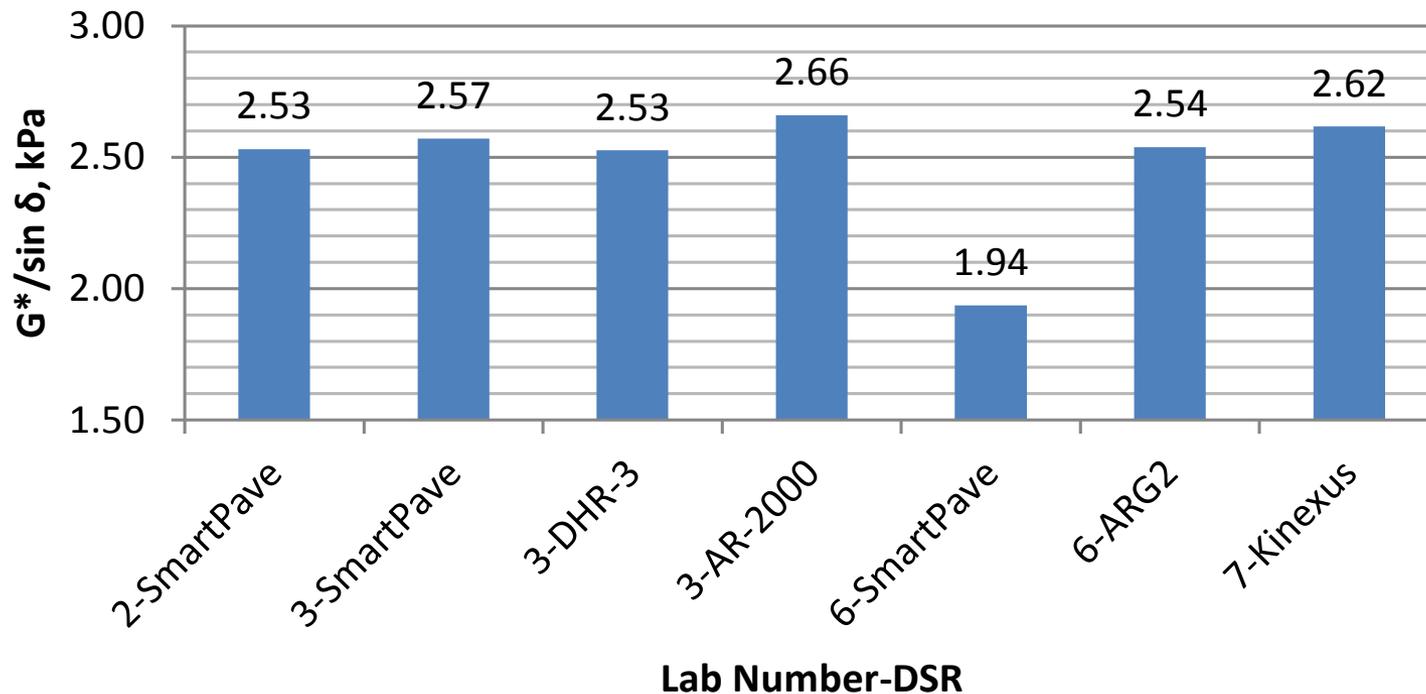


Jnr-3.2 Determined at T315 T_c: AAA

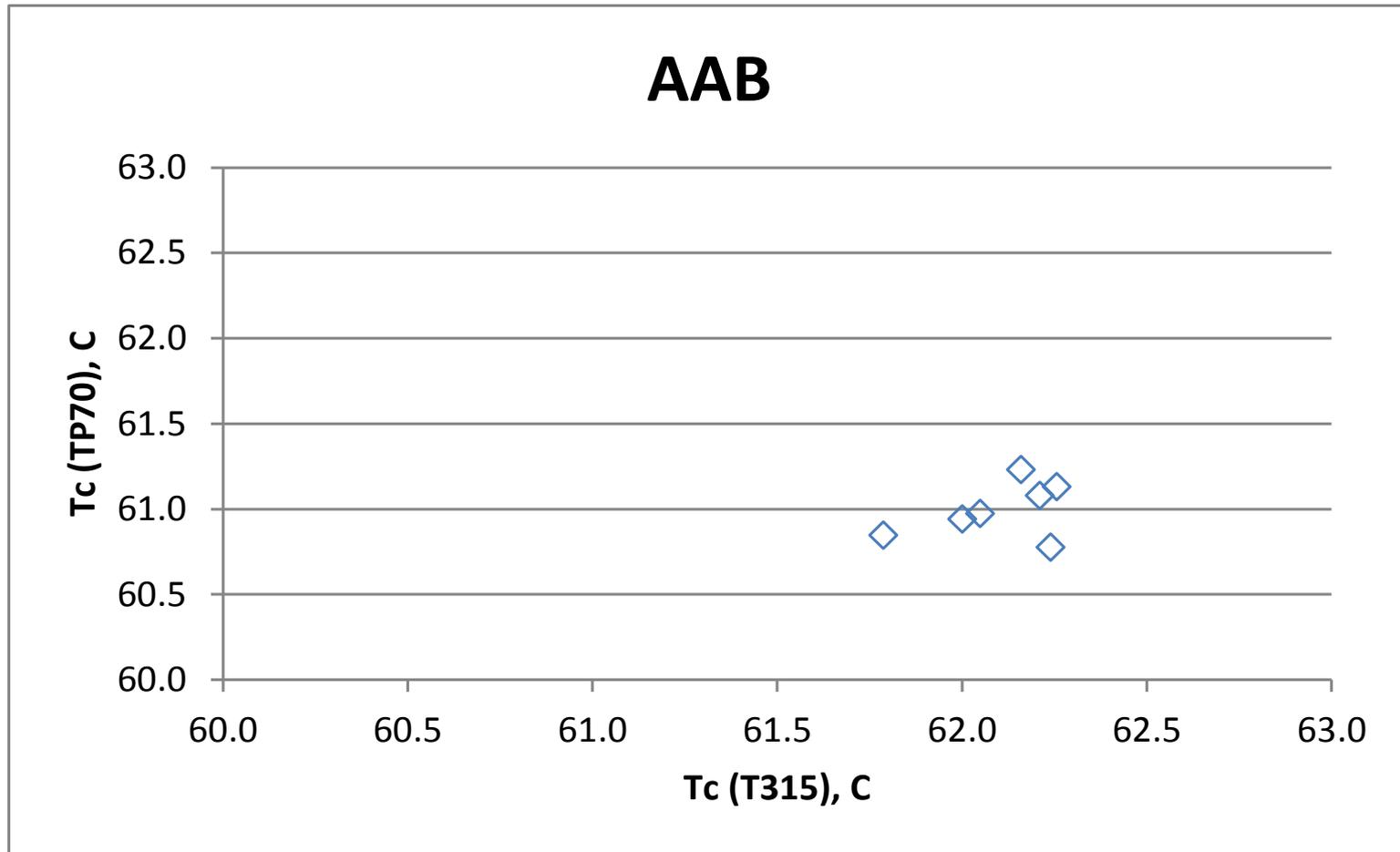


$G^*/\sin \delta$ Determined at TP70 T_c : AAA

AAA $G^*/\sin \delta$ @ T_c (Jnr-3.2)

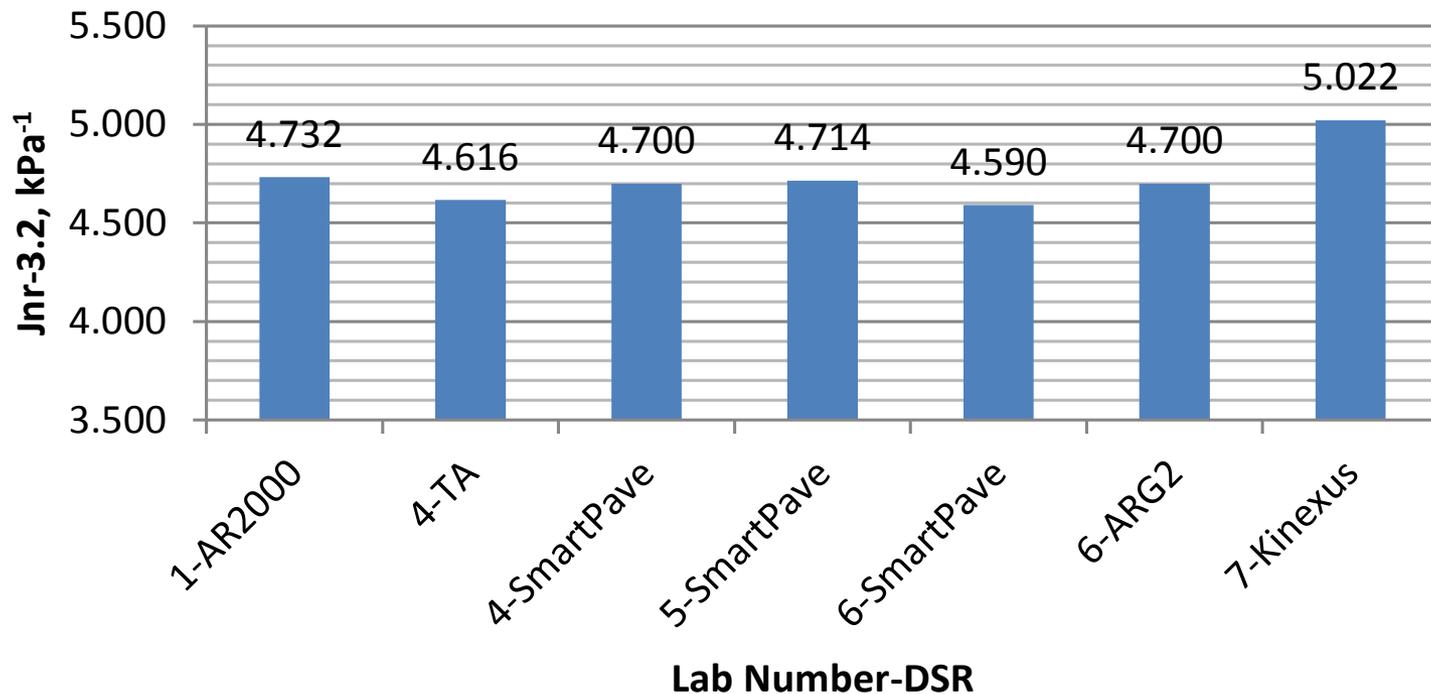


Comparison of T_c Determined by TP70 and T315: AAB



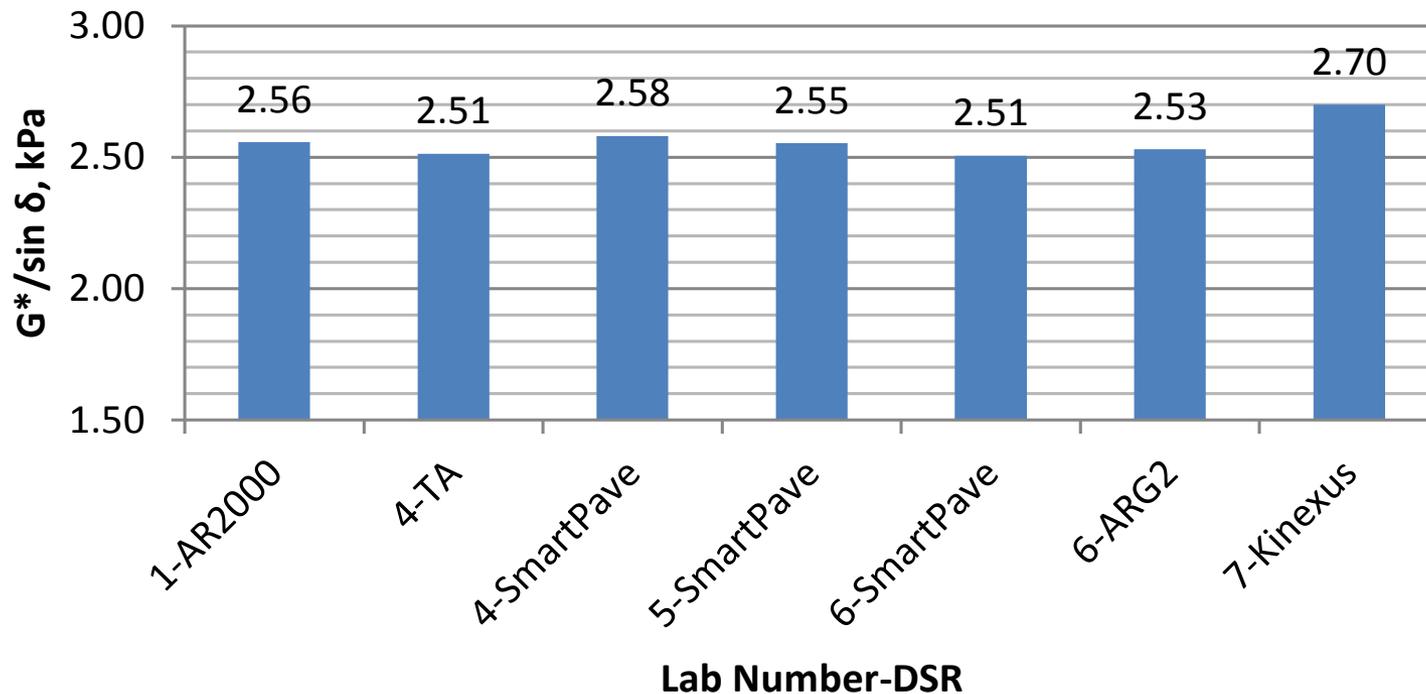
Jnr-3.2 Determined at T315 T_c: AAB

AAB Jnr-3.2 @ T_c(R-DSR)

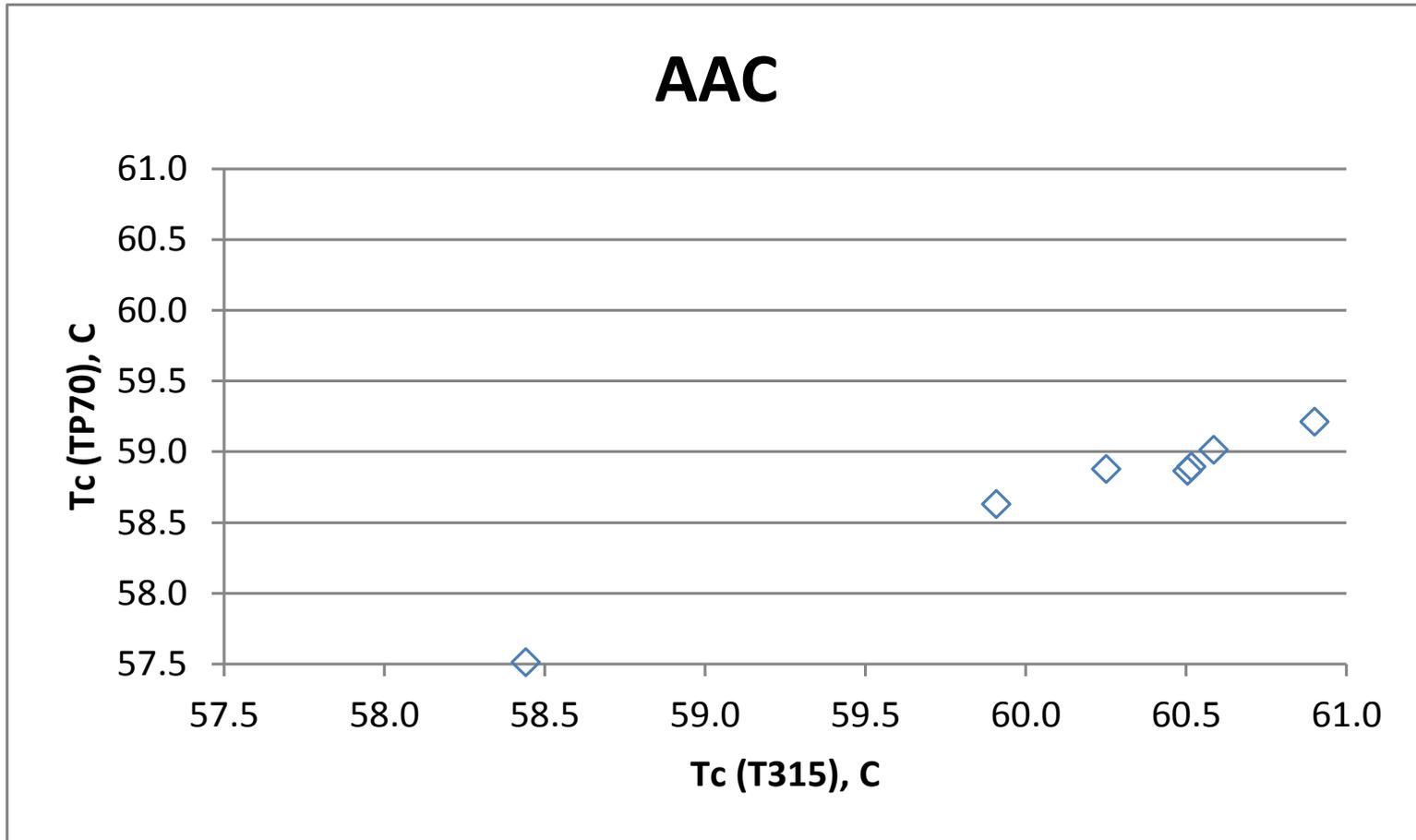


G*/sin δ Determined at TP70 T_c: AAB

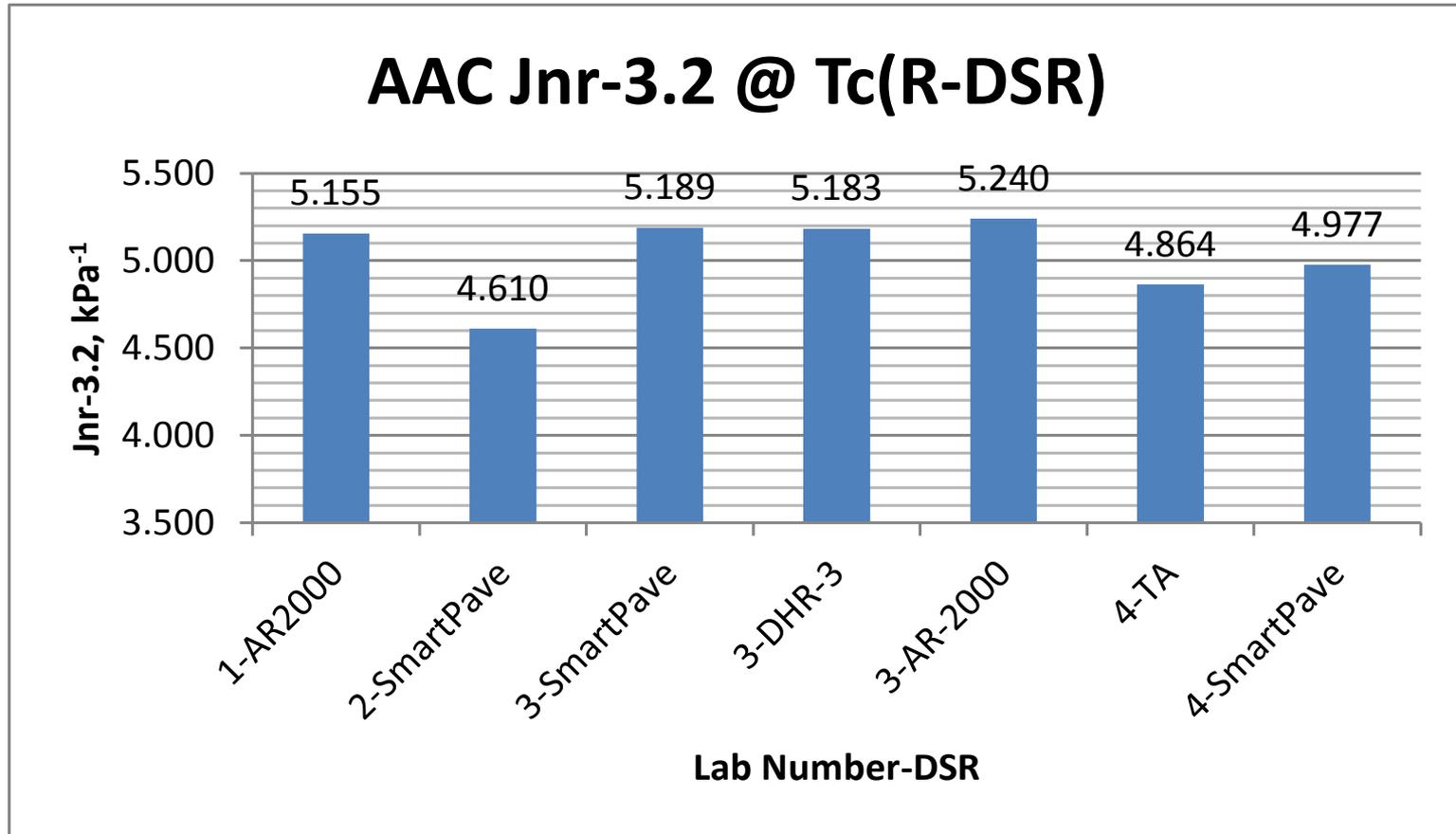
AAB G*/sin δ @ T_c(Jnr-3.2)



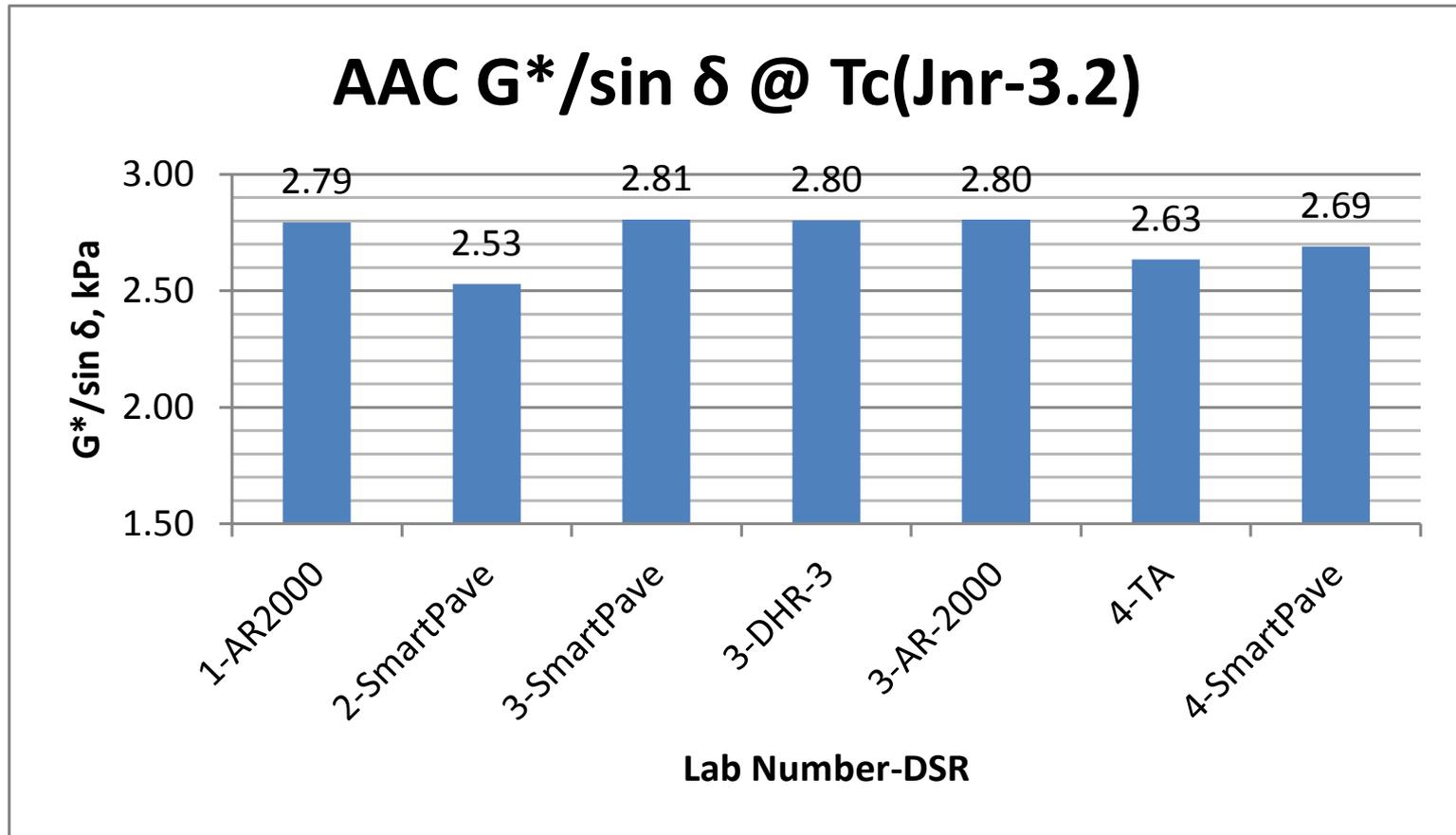
Comparison of T_c Determined by TP70 and T315: AAC



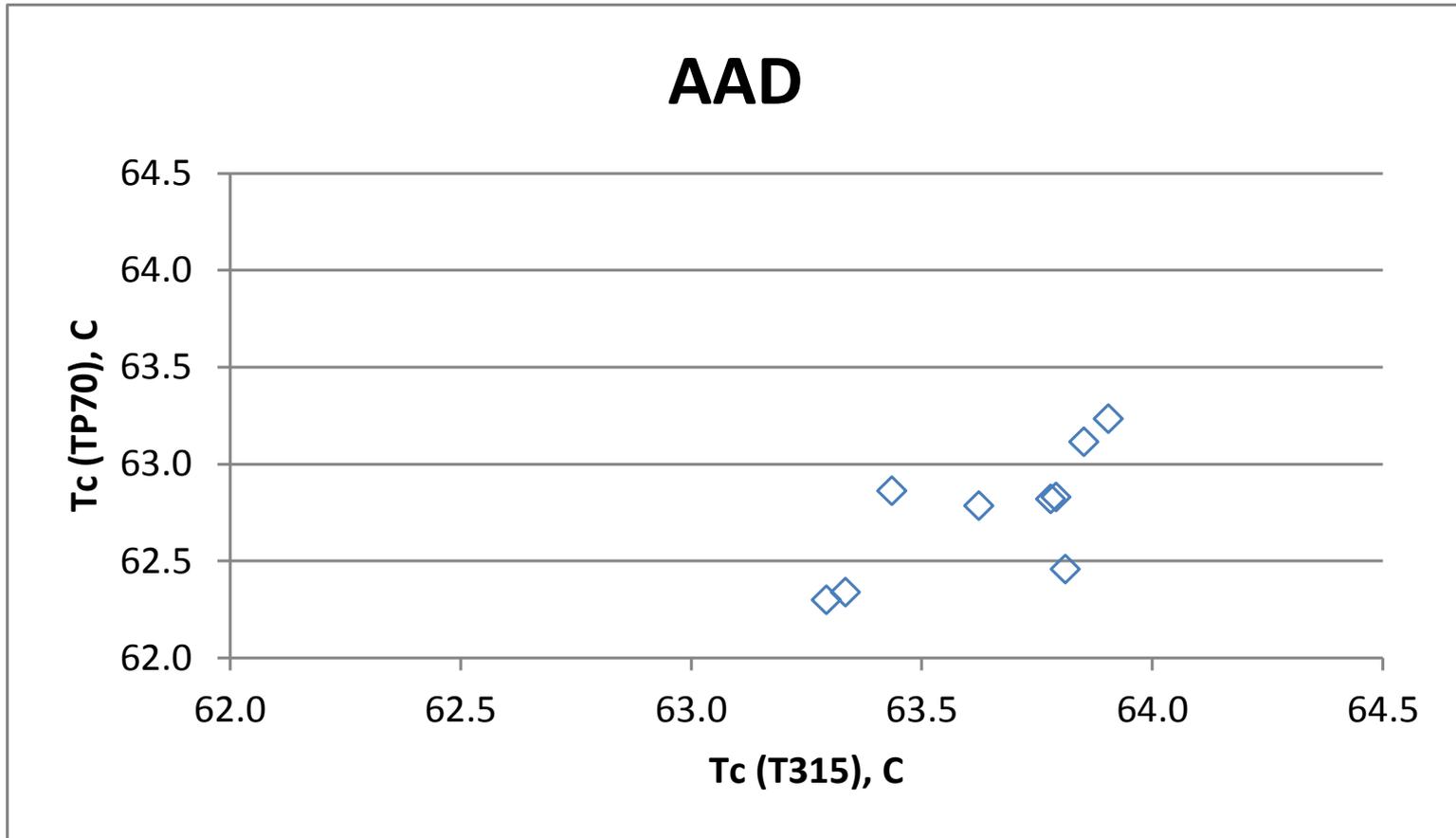
Jnr-3.2 Determined at T315 T_c: AAC



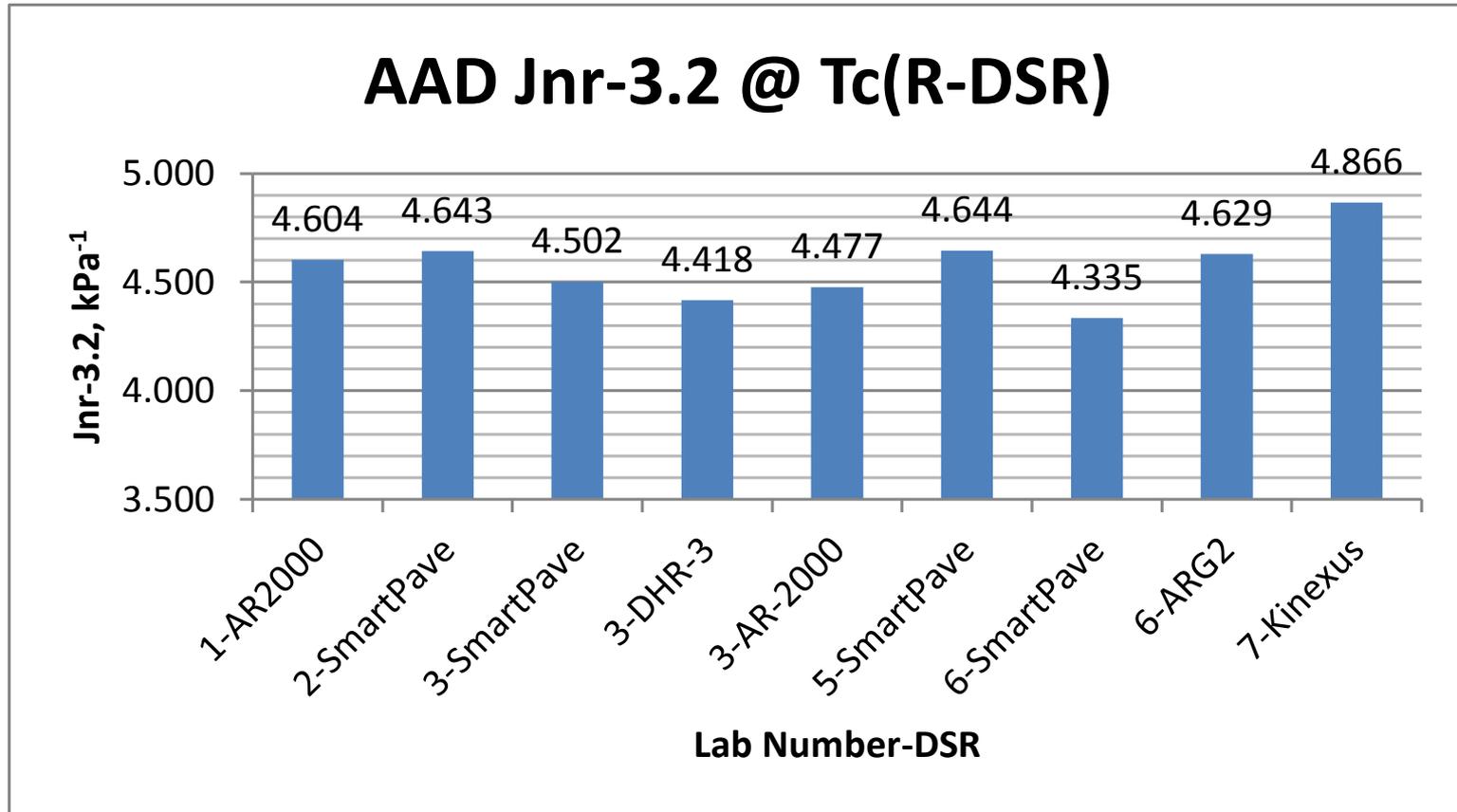
G*/sin δ Determined at TP70 T_c: AAC



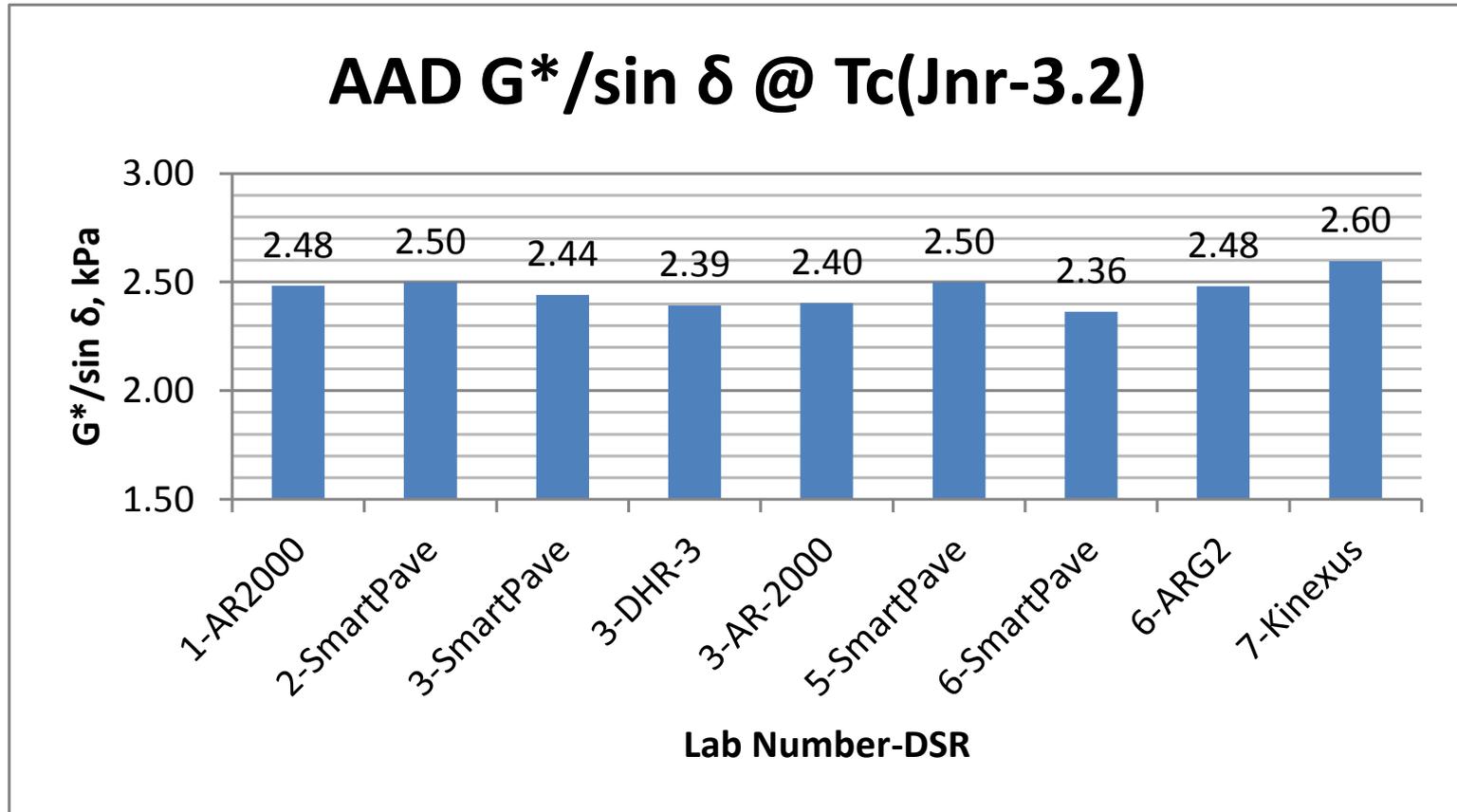
Comparison of T_c Determined by TP70 and T315: AAD



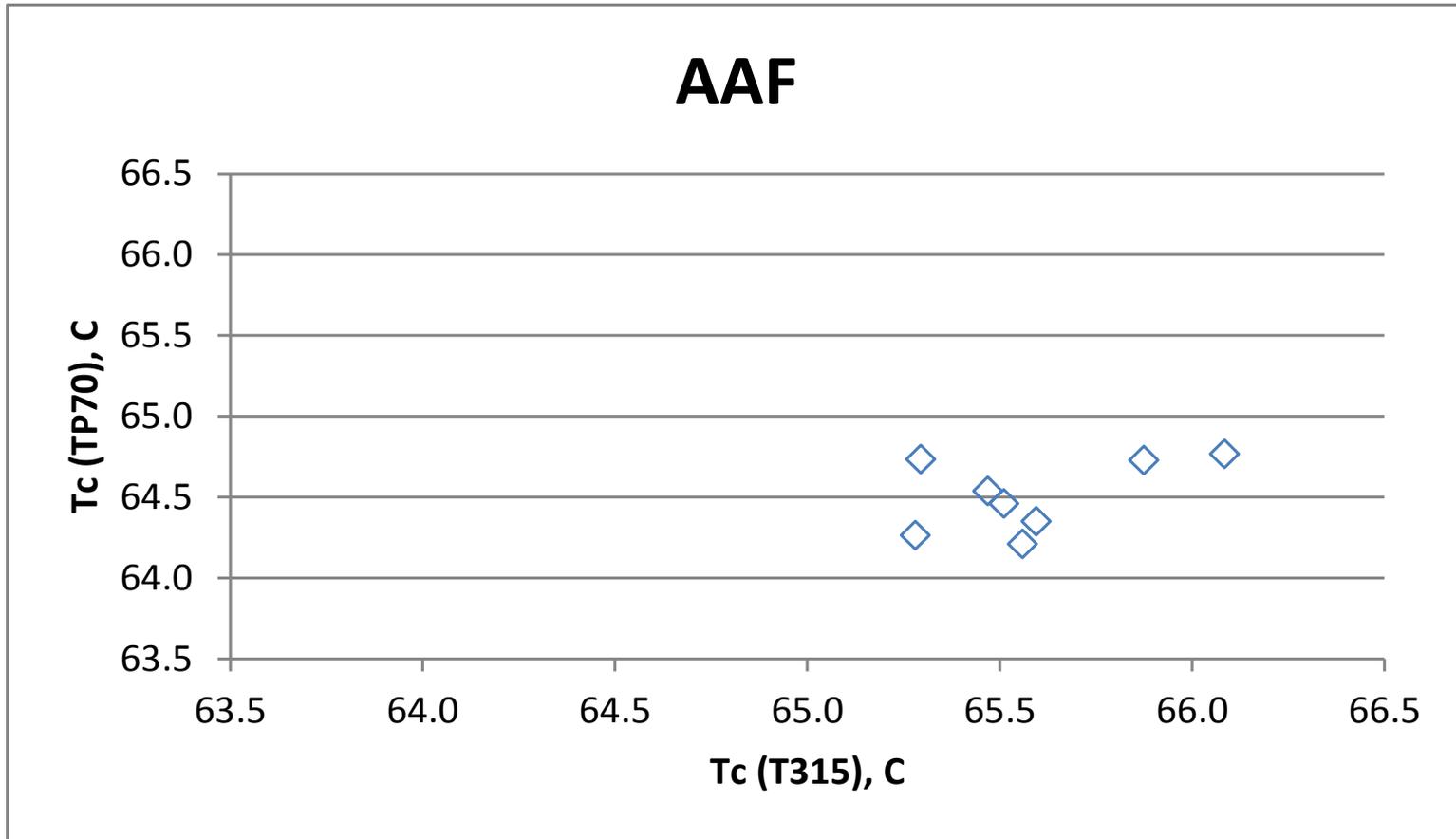
Jnr-3.2 Determined at T315 T_c: AAD



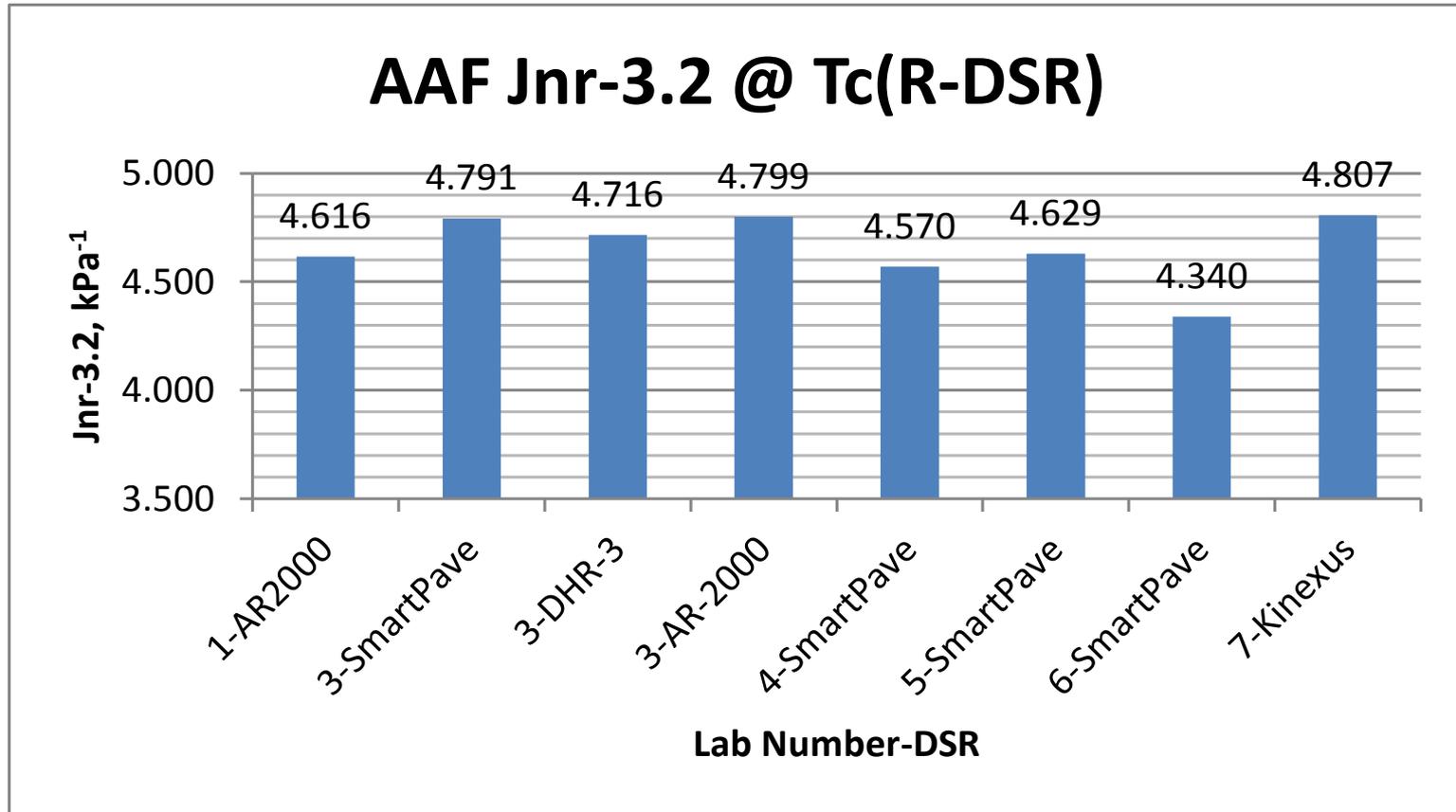
G*/sin δ Determined at TP70 T_c: AAD



Comparison of T_c Determined by TP70 and T315: AAF

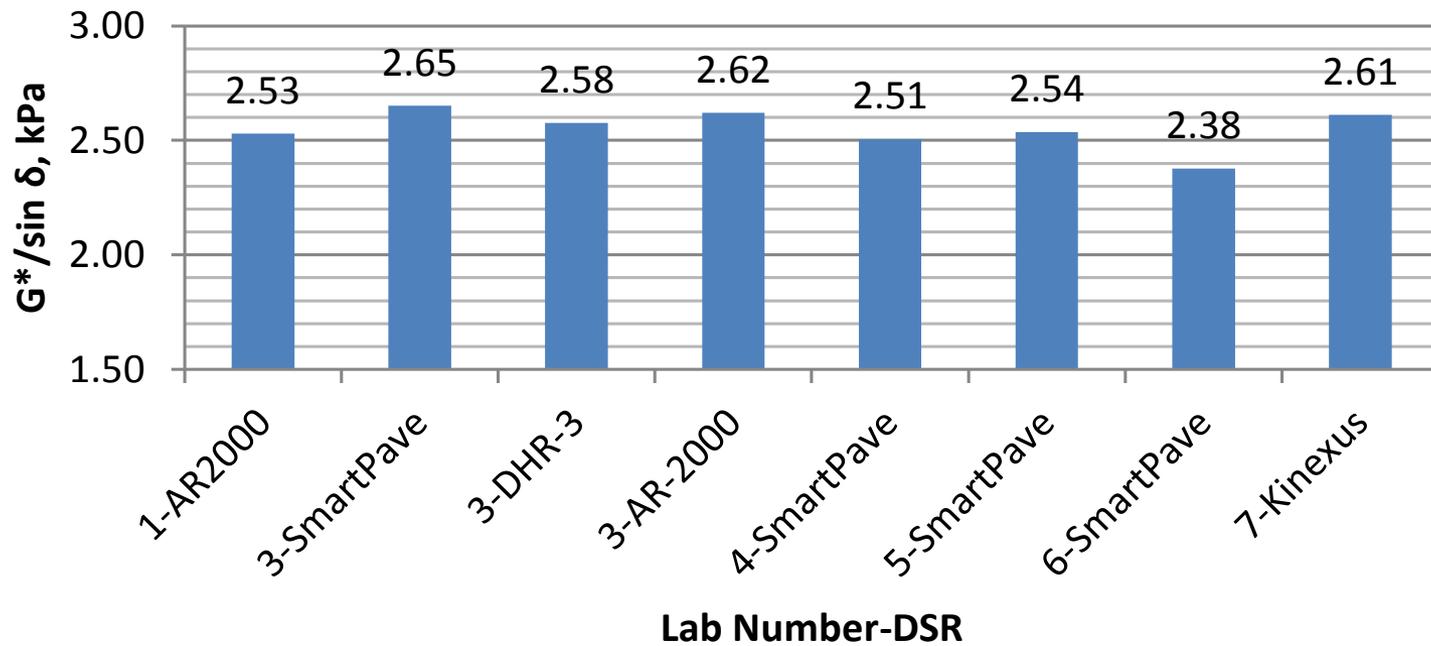


Jnr-3.2 Determined at T315 T_c: AAF

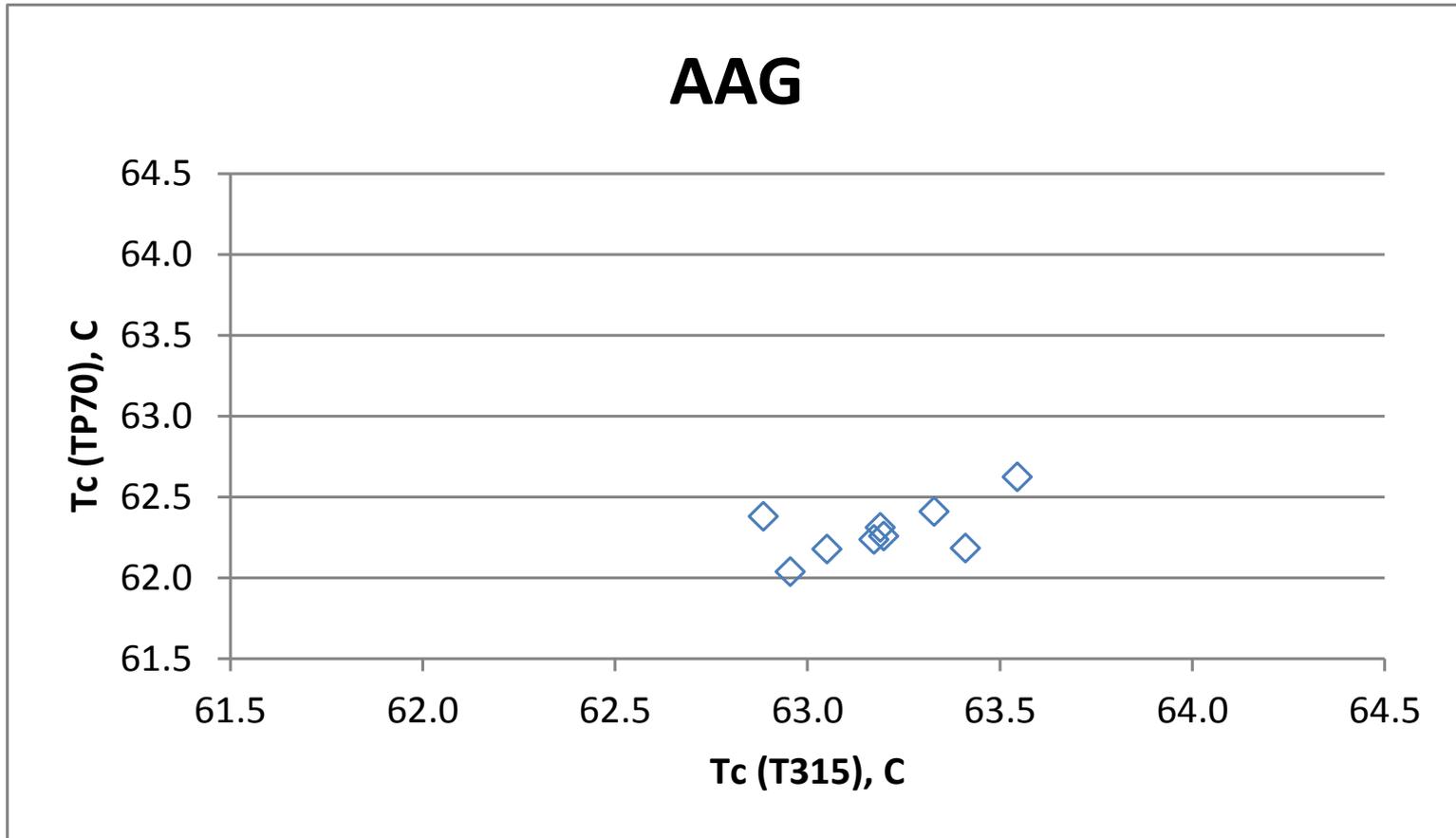


$G^*/\sin \delta$ Determined at TP70 T_c : AAF

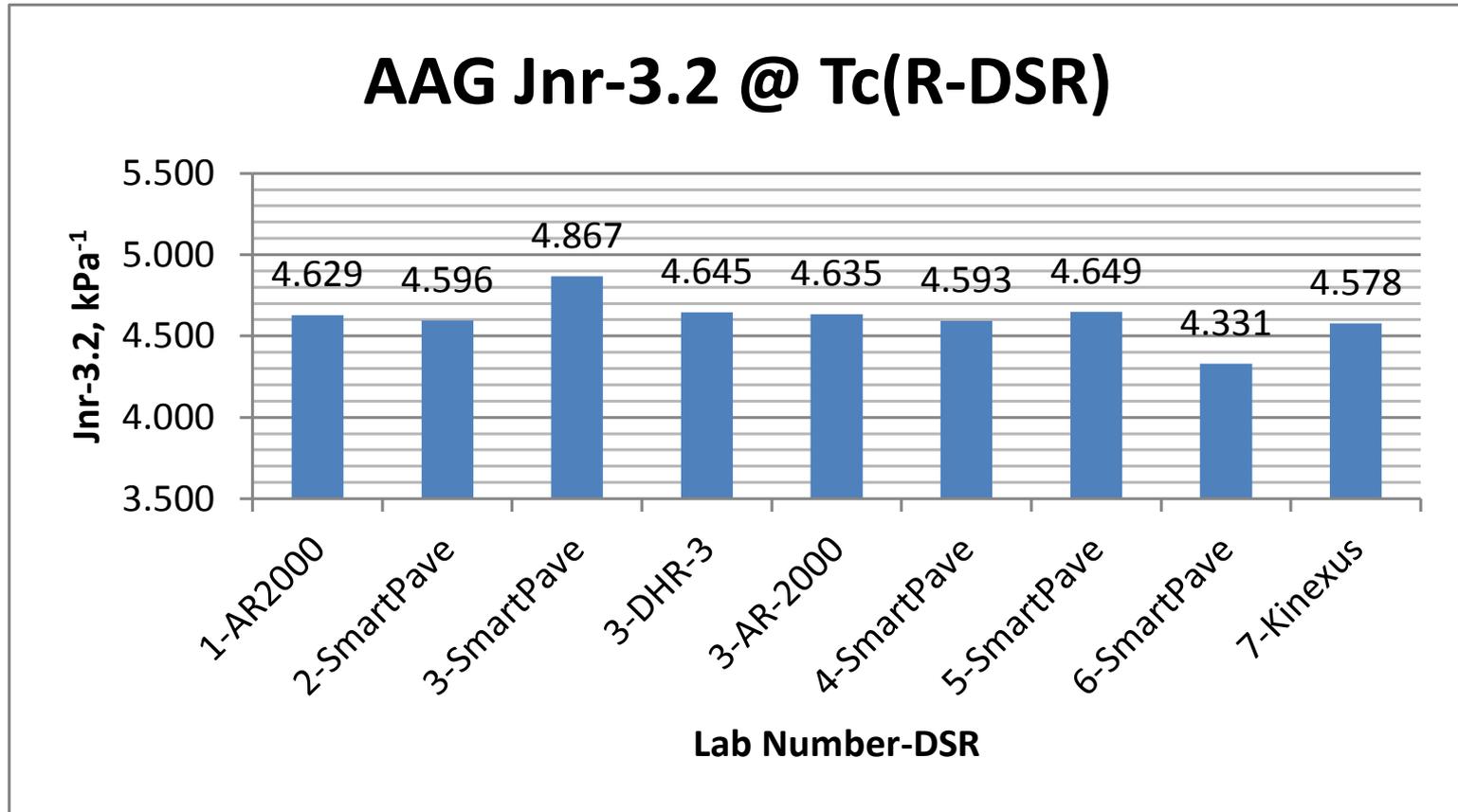
AAF $G^*/\sin \delta$ @ T_c (Jnr-3.2)



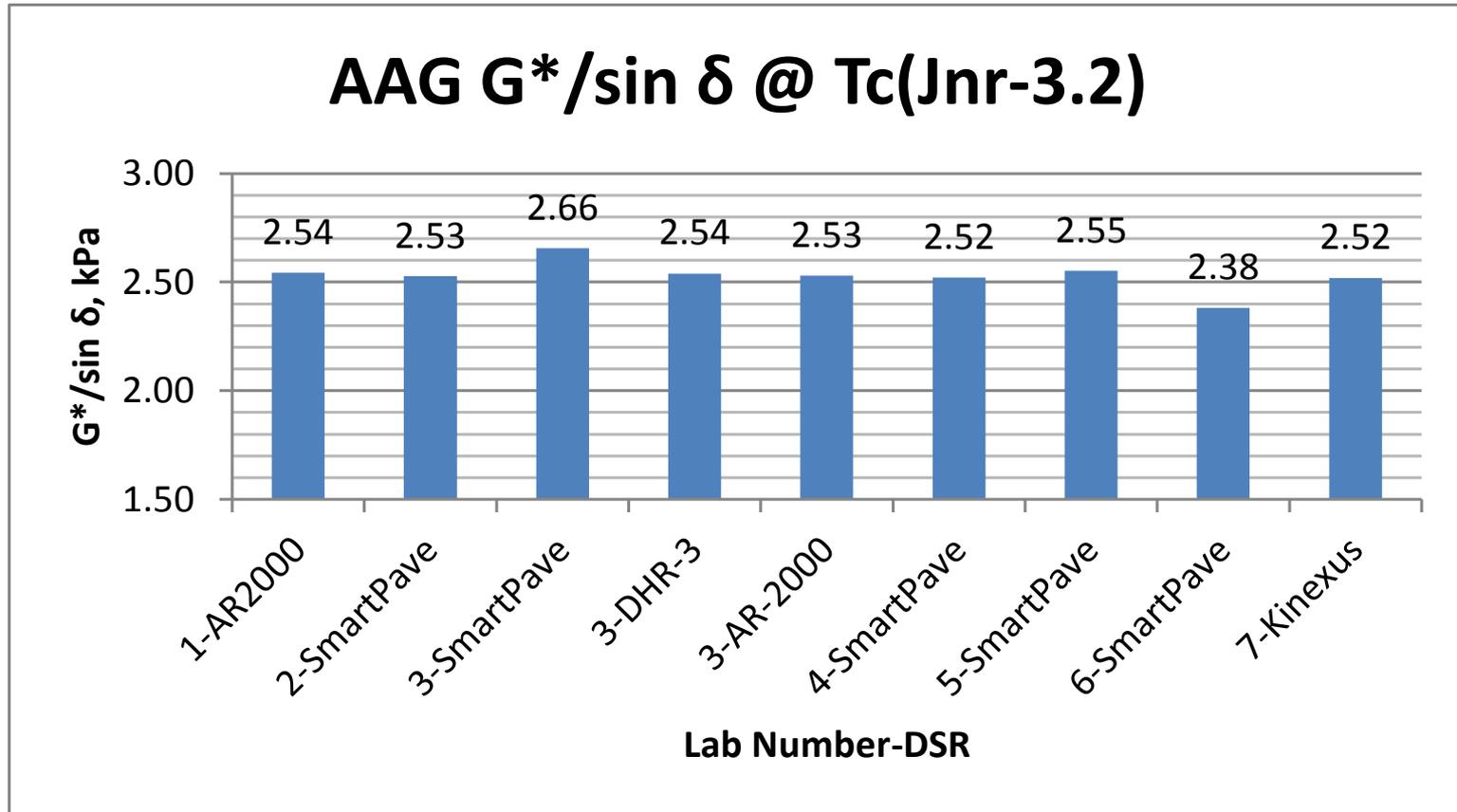
Comparison of T_c Determined by TP70 and T315: AAG



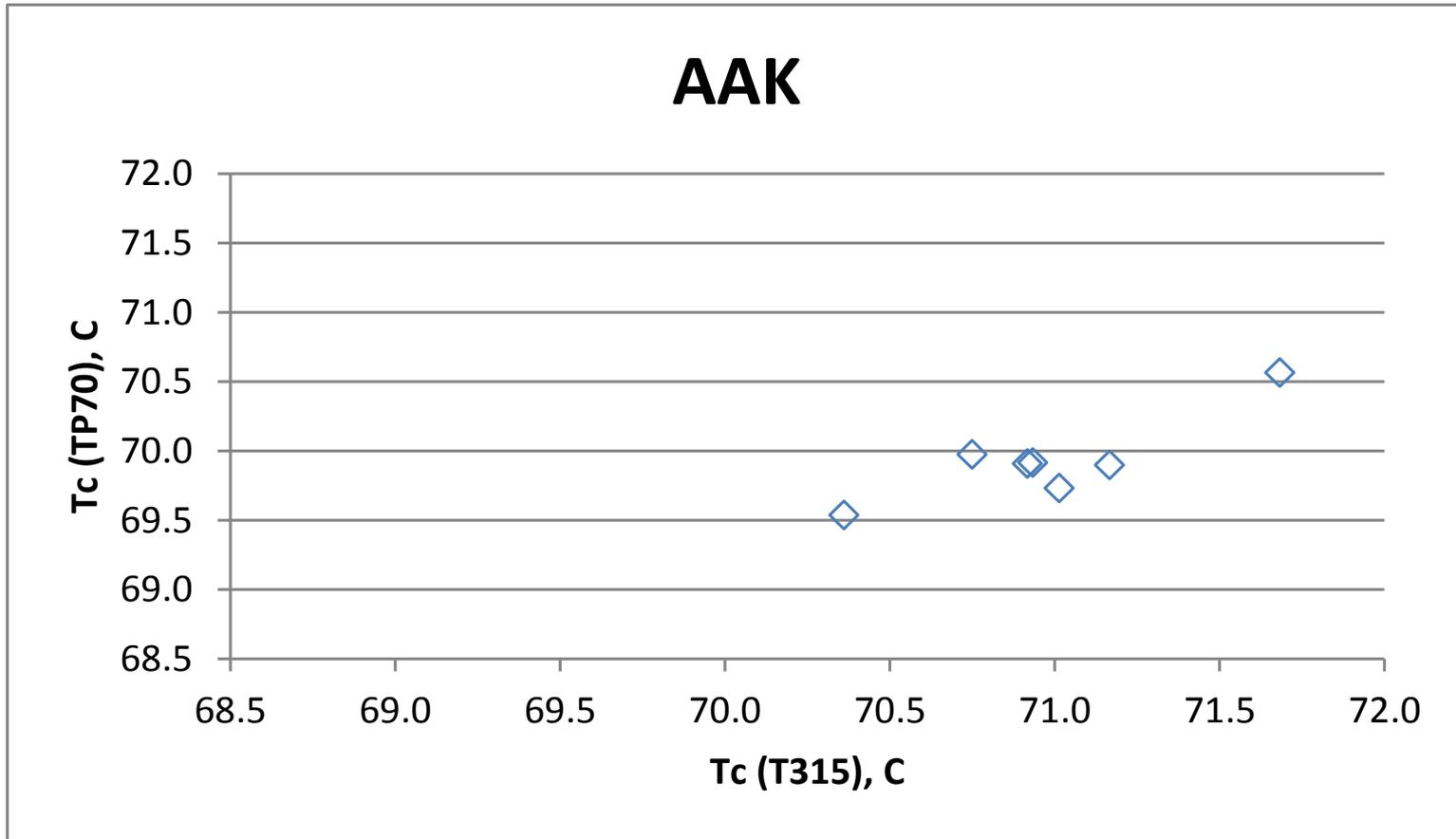
Jnr-3.2 Determined at T315 T_c: AAG



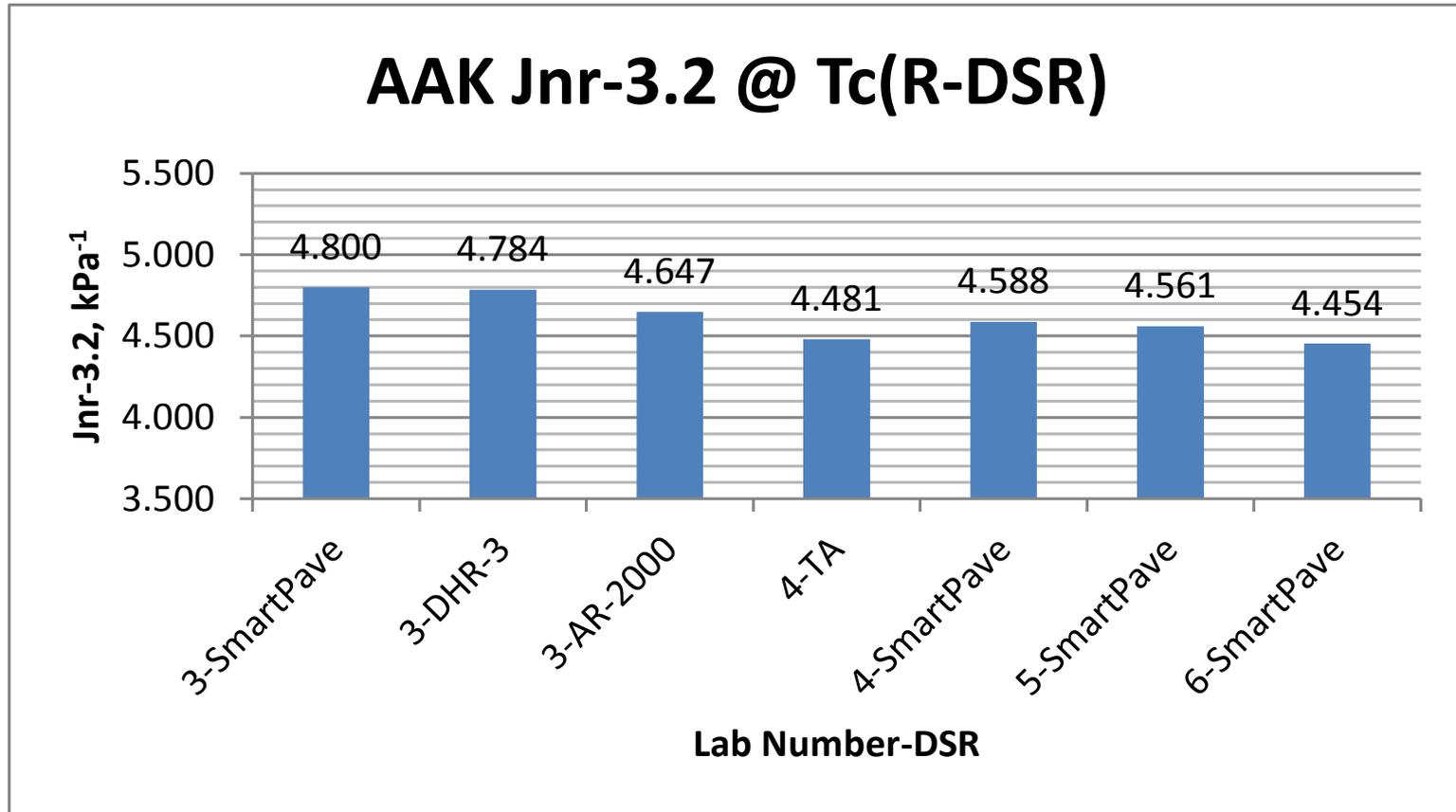
$G^*/\sin \delta$ Determined at TP70 T_c : AAG



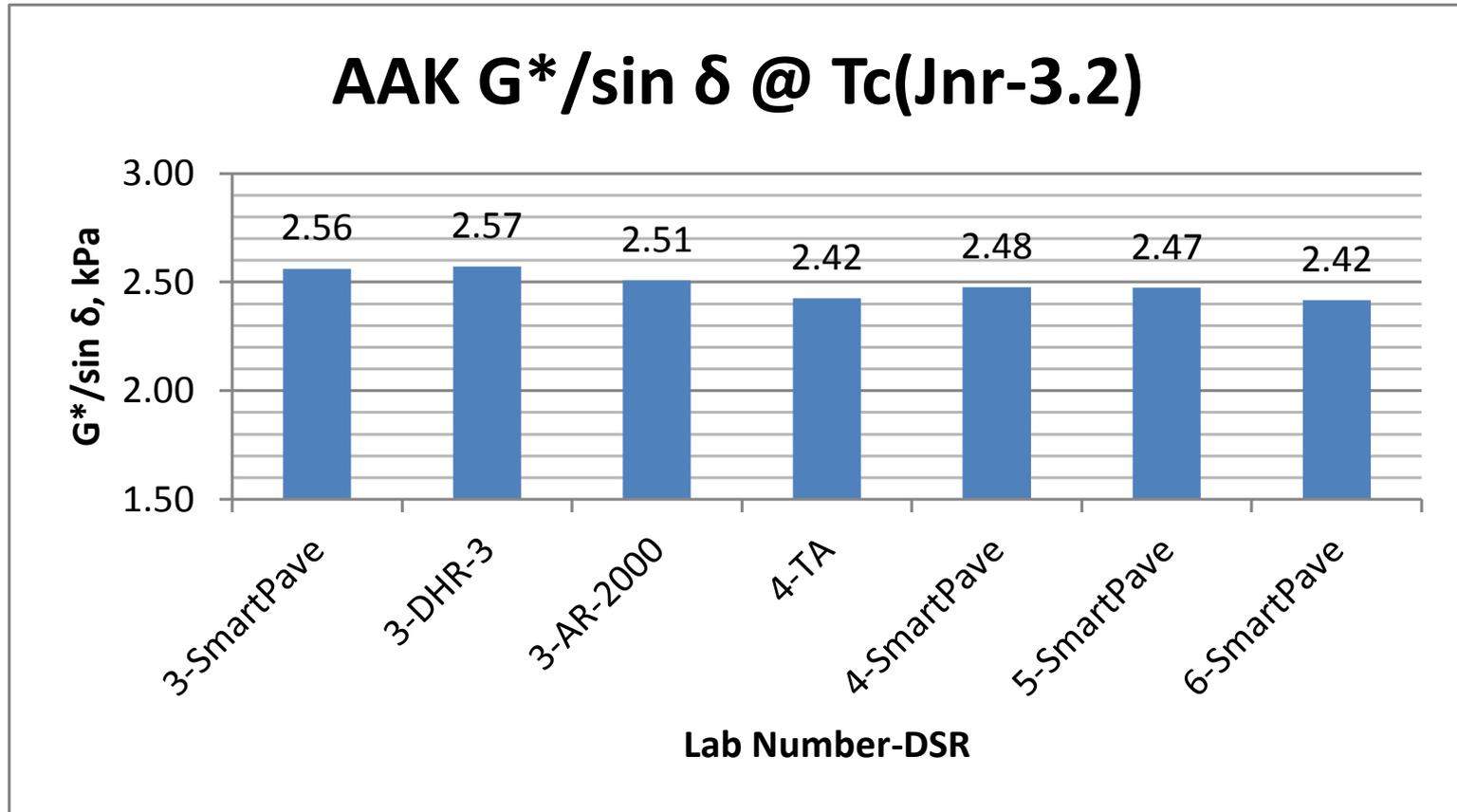
Comparison of T_c Determined by TP70 and T315: AAK



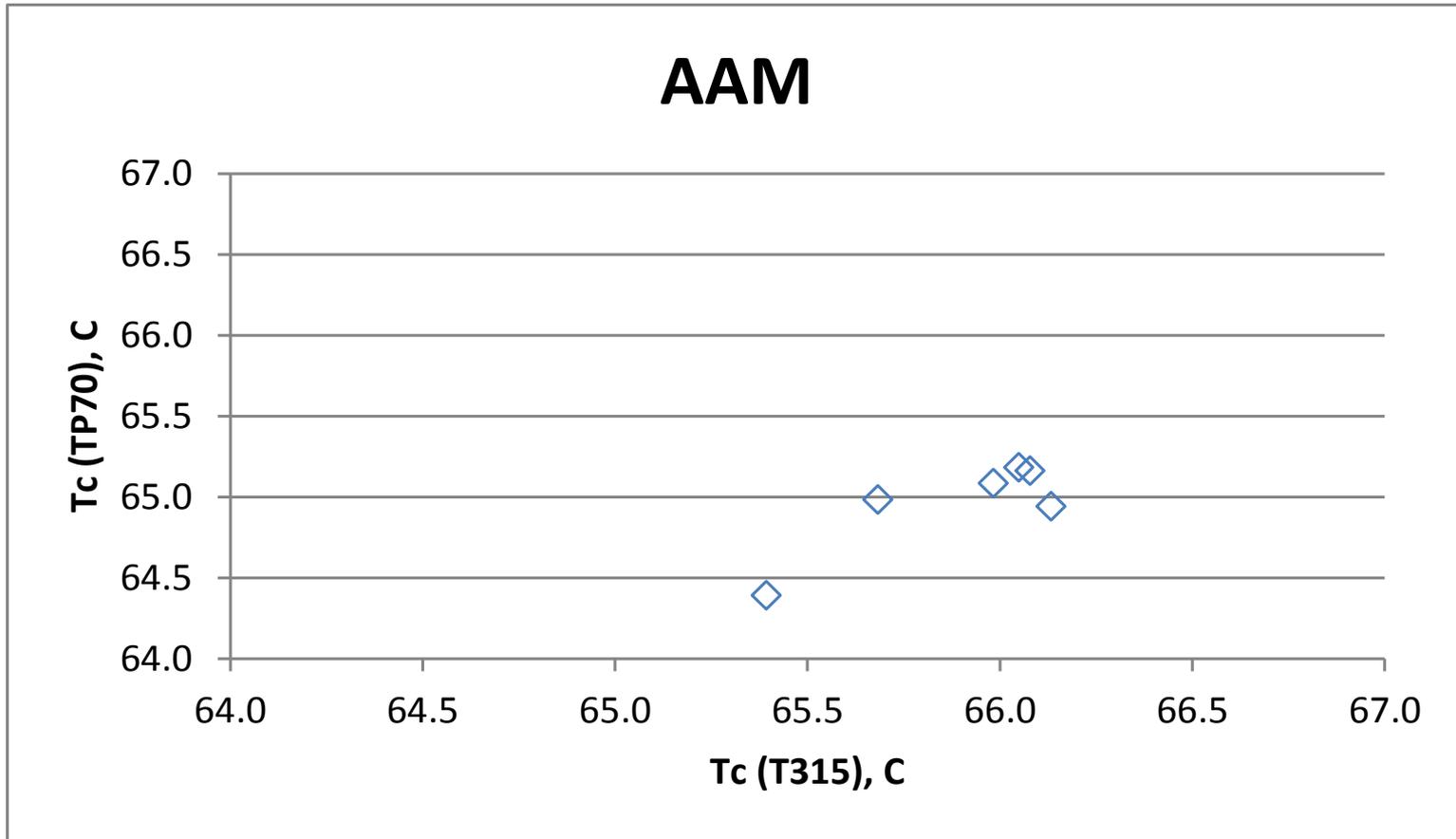
Jnr-3.2 Determined at T315 T_c: AAK



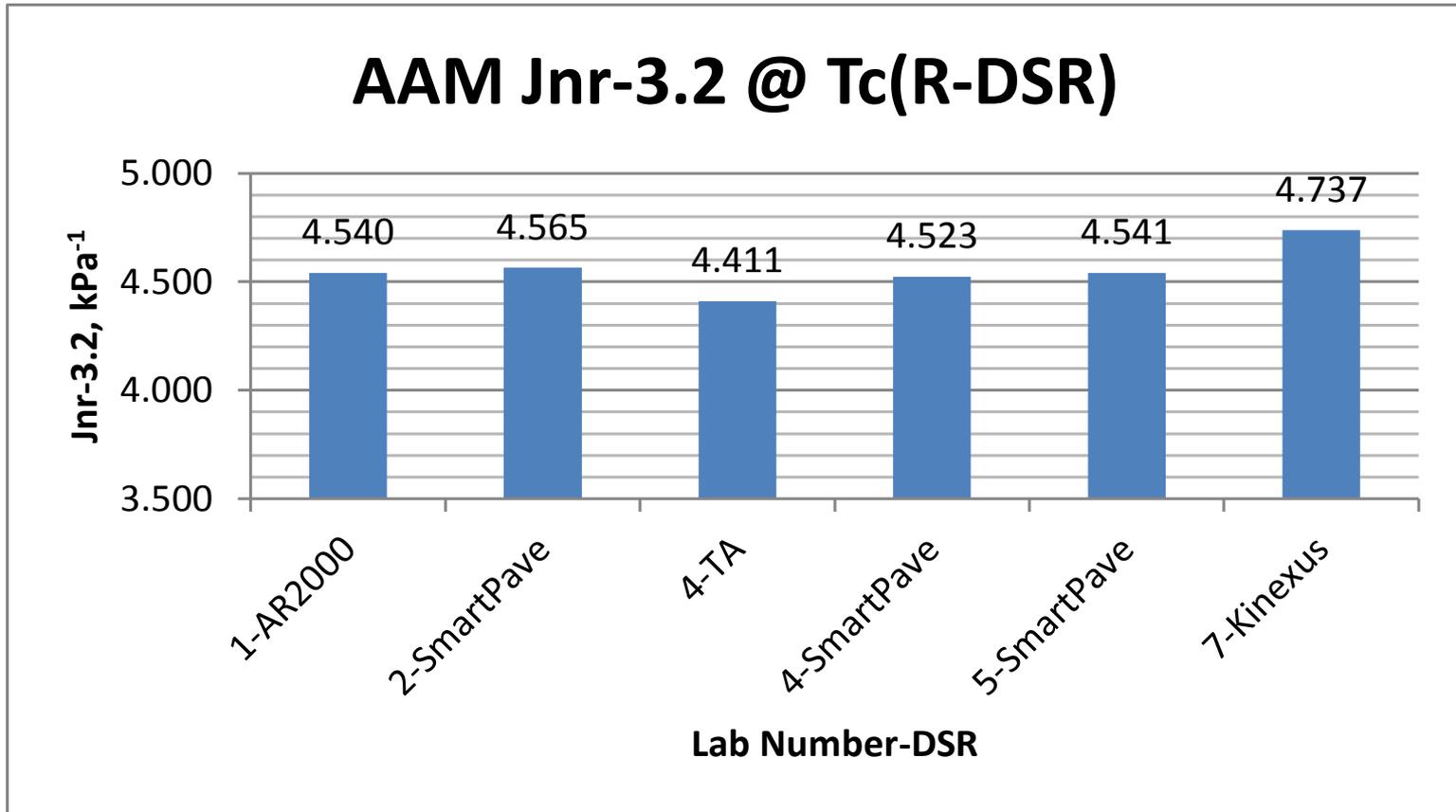
$G^*/\sin \delta$ Determined at TP70 T_c : AAK



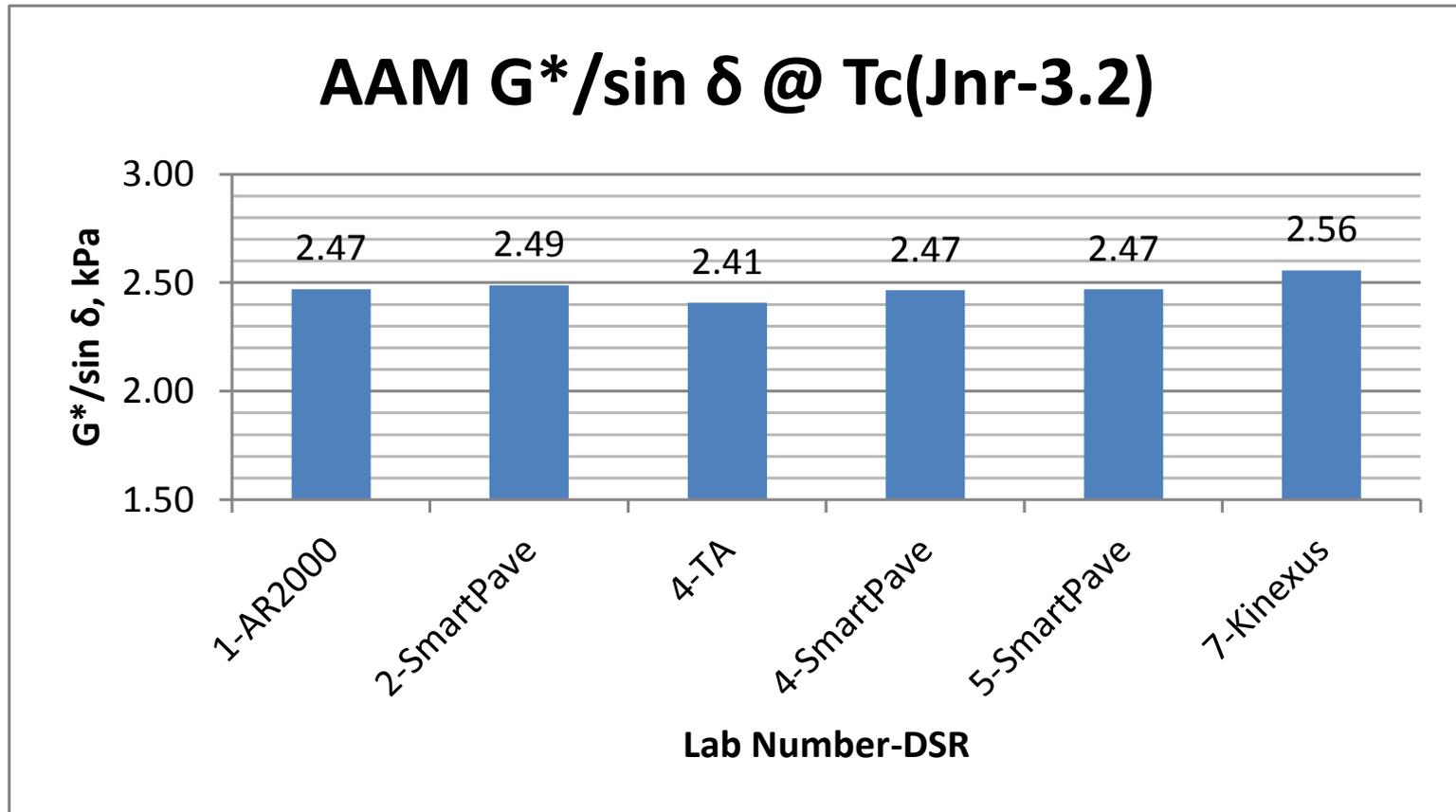
Comparison of T_c Determined by TP70 and T315: AAM

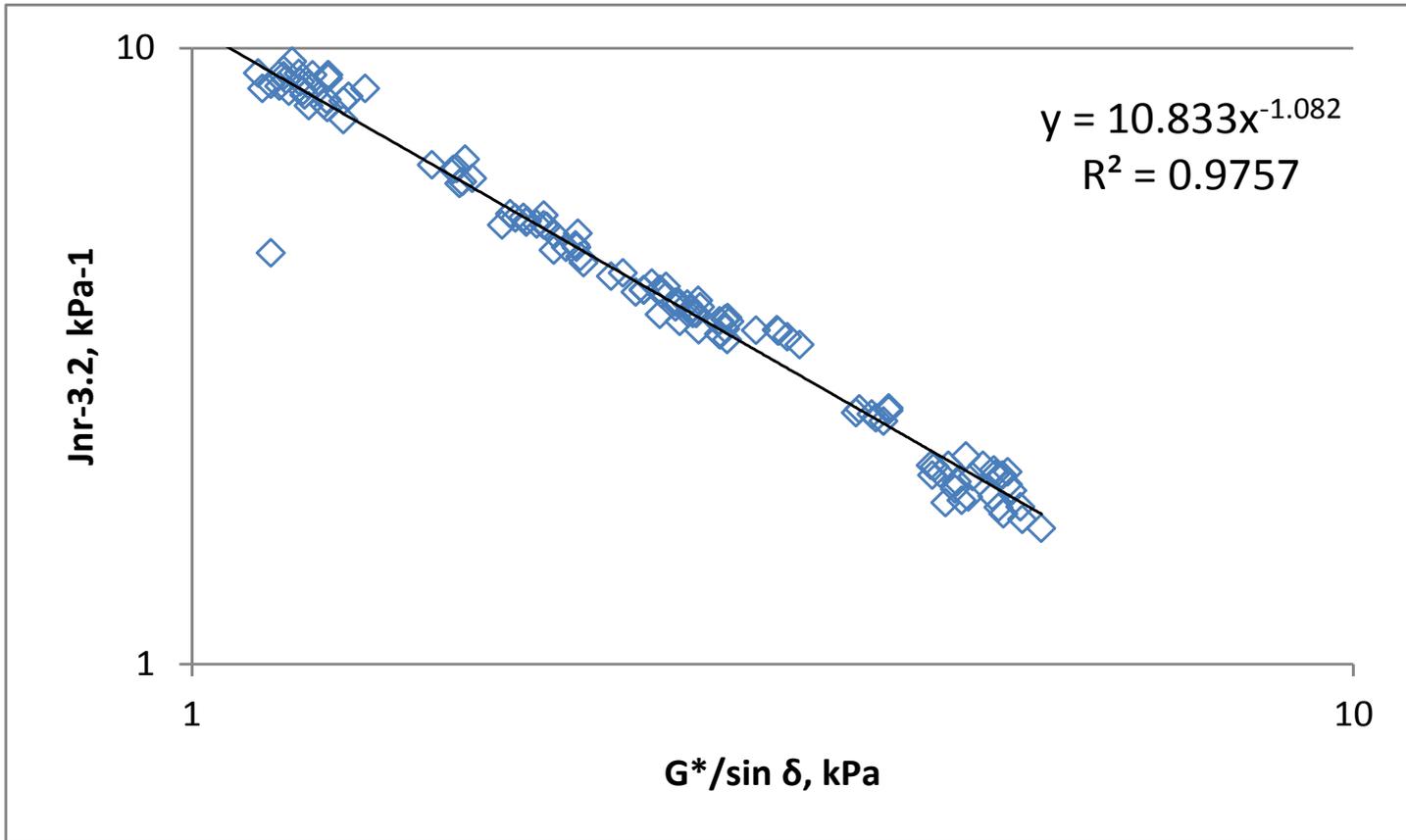


Jnr-3.2 Determined at T315 T_c: AAM



G*/sin δ Determined at TP70 T_c: AAM





A	10.833
B	-1.082
$G^*/\sin \delta$	2.2
Jnr-3.2	4.616
Jnr-3.2	4
$G^*/\sin \delta$	2.51



TAC Evaluation of SHRP MRL Asphalt Binders

- Summary
 - Evaluation Program
 - Eight Unmodified Asphalt Binders
 - Seven Participating Labs
 - Three DSR Manufacturers
 - $T_{c,Jnr}$
 - Consistently lower than $T_{c,G^*/\sin \delta}$
 - 0.5 – 1.7°C
 - Results generally confirm earlier findings
 - $T(R\text{-DSR}) = 4.62 \text{ kPa}^{-1}$
 - $T(Jnr\text{-3.2}) = 2.51 \text{ kPa}$



TAC Evaluation of SHRP MRL Asphalt Binders

- Summary
 - No evident bias in DSR manufacturer
 - Statistical analysis still needed
 - d2s% values similar for TP70 and T315
 - $G^*/\sin \delta$
 - Average: 12.1%
 - Range: 6.0% to 29.5%
 - Jnr-3.2
 - Average: 11.5%
 - Range: 4.6% to 24.6%



TAC Evaluation of SHRP MRL Asphalt Binders

- Next Steps
 - Present information to Asphalt Binder ETG
 - September 24-25, 2012
 - Minneapolis, MN
 - Recommendation from TAC
 - Should we recommend a change for AASHTO MP19 for “S” grades?
 - Jnr-3.2 = 4.5 kPa⁻¹ ?



AASHTO MP19 Criterion for Neat Asphalt Binders

- Asphalt Institute Technical Advisory Committee Recommendation
 - Recommend that the AASHTO MP19 criterion for J_{nr} for “S” graded asphalt binders be changed from 4.0 kPa^{-1} to 4.5 kPa^{-1} .
 - Mathematical exercise to allow unmodified asphalt binders graded by M320 to map directly over to MP19 grading with no change in properties.
 - Does not affect stiffness of currently produced unmodified asphalt binders



Thanks!

